Low Impact Development Cost Comparison

PREPARED FOR:

WSU Cooperative Extension Pierce County 3049 South 36th Street, Suite 300 Tacoma, WA 98409

PROJECT:

Low Impact Cost Comparison Pierce County, Washington

203386.30

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1.0 Introduction

AHBL Inc. was retained by WSU Cooperative Extension, Pierce County, to evaluate the relative construction costs between conventional development systems and Low Impact Development (LID) best management practices (BMP's). The project includes reviewing eight major development practices with several site variation scenarios. Each scenario is individually reviewed to develop an opinion of probable construction costs. It is important to note that these are simplified scenarios that may not include all the details that may be present on a particular site. These details include variations such as topographic relief, soil conditions, groundwater conditions, and climatalogical conditions.

All hydrologic modeling has been performed utilizing the Western Washington Hydrology Model as developed by the Washington State Department of Ecology (DOE). Existing conditions for detention size determination are all modeled as forests in good condition as required by the 2003 Department of Ecology *Stormwater Management Manual for Western Washington* (Stormwater Manual). Analysis of lot-scaled BMP's are based on a 5000 square foot lot with 2,000 square feet of roof coverage, 500 square feet of driveway and 2,500 square feet of turf/landscaping.

Cost provided are based on initial construction and do not include life cycle analysis or annual maintenance costs.

2.0 BIORETENTION CELL VS. INFILTRATION TRENCHES

This analysis consists of comparing the relative construction costs of underground infiltration trenches versus bioretention cells for managing stormwater runoff from equivalent tributary areas. For this analysis, several scenarios have been considered including different tributary area characteristics (i.e. roof runoff, driveway runoff) and different soil types (outwash soils, till soils). For BMP's it is assumed that a minimum of three feet of separation from the bottom of the facility to the seasonal high groundwater elevation or hardpan can be maintained.

For infiltration trenches, it is assumed that the void ration of the washed rock is approximately 30 percent. Infiltration through the sidewalls of the trench is neglected. The maximum ponding depth in bioretention swales is 6 inches. The systems have been designed to infiltrate 100 percent of the anticipated runoff for all storm events as predicted by WWHM. It should be noted that bioretention cells are typically not designed for 100 percent infiltration of the larger storm events. However, this method was chosen to enable a direct comparison with infiltration trenches which are, in most cases, designed to infiltrate all storm events. The comparisons will be similar for analysis completed to infiltrate a lesser percentage of all predicted stormwater runoff volumes.



2.1 Roof Runoff, Outwash Soils

The is scenario compares the cost of infiltration trenches versus bioretention cells for management of roof runoff from a standard residential roof (2000 square feet) for a site with outwash soils. The stormwater runoff in this case does not require treatment prior to infiltration.

	Item	Unit Cost	Quantity	Cost
Infiltration Trench			-	
	Washed Rock	\$20/CY	5 CY	\$100.00
	4" Perf. Pipe	\$8/LF	15 LF	\$120.00
	Catch Basin	\$700/EA	1 EA	\$700.00
	Excavation	\$4.50/CY	5 CY	\$22.50
			Total _	\$942.50
Bioretention Cell				
	Soil Mix	\$25/CY	25 CY	\$625.00
	Planting	\$1/SF	450 SF	\$450.00
	Mulch	\$20/CY	4 CY	\$80.00
	Excavation	\$4.50/CY	25 CY	\$112.50
			Total	\$1,267.50
			Difference	\$325.00

2.2 Roof Runoff, Till Soils

This scenario matches the previous scenario with the exception of soil type. This scenario uses till soils in the modeling which has a lower infiltration rate than outwash soils. Note that the size of the bioretention swale has not changed from the outwash to the till condition. This study assumes that the infiltration rate of bioretention soil mix is similar to underlying till soils and therefore restricts the infiltration rate in the outwash soils. An assumed infiltration rate for the bioretention soil mix of 1 inch per hour was utilized for stormwater modeling. Infiltration rates ranging from 1 to 2.4 inches per hour are commonly used for bioretention cells.

	Item	Unit Cost	Quantity	Cost
Infiltration Trench				
	Washed Rock	\$20/CY	33 CY	\$660.00
	4" Perf. Pipe	\$8/LF	100 LF	\$800.00
	Catch Basin	\$700/EA	2 EA	\$1400.00
	Filter Fabric	\$0.50/SF	900 SF	\$450.00
	Excavation	\$4.50/CY	33 CY	\$148.50
			Total _	\$3,458.50
Bioretention Cell				
	Soil Mix	\$25/CY	25 CY	\$625.00
	Planting	\$1/SF	450 SF	\$450.00
	Mulch	\$20/CY	4 CY	\$80.00



Excavation	\$4.50/CY	25 CY	\$112.50
		Total _	\$1,267.50
		Difference	\$2,191.00

2.3 Driveway Runoff, Outwash Soils

The third scenario analyzes infiltration facility requirement for driveway runoff. For this scenario the standard driveway area is considered to be 500 square feet. Infiltration trenches are typically not recommended for infiltration of runoff from pollution generating impervious surfaces in outwash soils because of the limited treatment capacity of the underlying soils. Therefore, a separate treatment facility would be necessary prior to infiltration. There is an extensive range of treatment options that could be utilized depending on individual site conditions and the costs of these treatment options are highly variable. For the purposed of this analysis, it has been assumed that the project will utilize a catch basin type treatment unit similar to the catch basin filter manufactured by Stormwater Management Inc. Stormwater treatment in a bioretention cell is provided by plant uptake and the filtering of the stormwater through the bioretention soil mix.

	Item	Unit Cost	Quantity	Cost
Infiltration Trench				
	Washed Rock	\$20/CY	1.5 CY	\$30.00
	4" Perf. Pipe	\$8/LF	5 LF	\$40.00
	Treatment Catch Basin	\$2,000/EA	1 EA	\$2,000.00
	Filter Fabric	\$0.50/SF	45 SF	\$22.50
	Excavation	\$4.50/CY	1.5 CY	\$6.75
			Total _	\$2,099.25
Bioretention Cell				
	Soil Mix	\$25/CY	4 CY	\$100.00
	Planting	\$1/SF	68 SF	\$68.00
	Mulch	\$20/CY	.75 CY	\$15.00
	Excavation	\$4.50/CY	4 CY	\$18.00
			Total	\$201.00
			Difference	\$1,898.25

2.4 Driveway Runoff, Till Soils

This scenario is the same as the previous except the native soils are modeled as till soils. In this case, treatment is not required for runoff prior to infiltration in the infiltration trench because till soils have a greater pollutant removal capacity. For proper treatment to be achieved, three feet of separation must be maintained from the bottom of the trench to the seasonal high ground water elevation.



	Item	Unit Cost	Quantity	Cost
Infiltration Trench				
	Washed Rock	\$20/CY	8 CY	\$160.00
	4" Perf. Pipe	\$8/LF	25 LF	\$200.00
	Catch Basin	\$700/EA	1 EA	\$700.00
	Filter Fabric	\$0.50/SF	225 SF	\$112.50
	Excavation	\$4.50/CY	8 CY	\$36.00
			Total _	\$1,208.50
Bioretention Cell				·
	Soil Mix	\$25/CY	6 CY	\$90.00
	Planting	\$1/SF	112 SF	\$112.00
	Mulch	\$20/CY	1 CY	\$20.00
	Excavation	\$4.50/CY	6 CY	\$27.00
			Total _	\$309.00
			Difference	\$899.50

As described above, the size of the bioretention cell does not vary from till soils to outwash soils based on the infiltration rate assumptions made for this study.

3.0 STANDARD ROAD VS. LID ROAD SECTION

This section reviews the construction costs differences between a standard 24-foot asphalt pavement road section with curb and gutter and closed conveyance and a LID road section with 24 feet of pavement but bioretention swales replace the curb and gutter and closed conveyance system. The analysis has been performed on a typical 1000 foot length of road. This analysis does not include site specific cost parameters such as clearing requirements, rough grading, erosion control BMP's, etc.

3.1 Standard Road Section

The standard road section consists of 24-feet of crowned asphalt concrete pavement with curb and gutter on each side. Average catch basin spacing is assumed to be 250 feet and all storm conveyance pipes are 12-inches in diameter. A 5-foot concrete sidewalk is provided on each side of the road. The assumed asphalt section is 2 inches of Class B asphalt over 2 inches of crushed surfacing top course (CSTC) and 6 inches of gravel base. The detention volume required for 1000 feet of road is 27,617 cubic feet and the treatment volume is 6011 cubic feet. For cost comparisons, it is assumed that stormwater management is provided by a combination wetpond with live detention storage. Detention and treatment volumes include runoff from adjacent driveways. The project assumes forty driveways along the 1000-foot length of road with a standard area of 500 square feet each.



3.2 LID Road Section

The LID road section consists of 24-feet of crowned asphalt concrete pavement with bioretention swales on each side in place of curb and gutter. A 4-foot grass shoulder is provided between the edge of the paved surface and the bioretention swale. The swale is intercepted by 20 foot wide residential driveways every 50 feet on center. A 12-inch culvert, 25 feet long, is provided under each driveway. A 5-foot concrete sidewalk is provided on each side of the road behind the proposed swales. The assumed asphalt section is the same as the standard road section. The stormwater modeling shows that the bioretention swale adequately infiltrates over 96-percent of the total stormwater runoff from the road and driveway surfaces. However, the swales are unable to meet the runoff rate and duration standards for large storm events. Therefore, a detention facility will be required after the swales. Because the swales infiltrate 96-percent of the runoff, exceeding the 91-percent storm treatment volume required by the Storm Manual, additional runoff treatment is not required.

3.3 Cost Summary

	Item	Unit Cost	Quantity	Cost
Standard Road Section				
	Class B Asphalt (2")	\$35/CY	148 CY	\$5,180.00
	CSTC (2")	\$15/CY	148 CY	\$2,220.00
	Gravel Base (6")	\$12/CY	444 CY	\$5,328.00
	Curb & Gutter	\$15/LF	2,000 SF	\$30,000.00
	Sidewalk	\$30/SY	1,111 SY	\$33,330.00
	Storm CB	\$700/EA	8 EA	\$5,600.00
	12" CPEP Storm	\$18/LF	950 LF	\$17,100.00
	Treatment Volume	\$4.50/CY	223 CY	1,003.50
	Detention Volume	\$4.50/CY	1,025 CY	4,612.50
			Total	\$104,374.0
				0
LID Road Section				
	Soil Mix	\$25/CY	160 CY	\$4000.00
	Swale Planting	\$1/SF	2,880 SF	\$2,880.00
	Mulch	\$20/CY	30 CY	\$60.00
	Swale Excavation	\$4.50/CY	760 CY	\$3,420.00
	Class B Asphalt (2")	\$35/CY	148 CY	\$5,180.00
	CSTC (2")	\$15/CY	148 CY	\$2,220.00
	Gravel Base (6")	\$12/CY	444 CY	\$5,328.00
	Sidewalk	\$30/SY	1,111 SY	\$33,330.00
	12" Culverts	\$18/LF	720 LF	\$12,960.00
	4" Perf. Pipe	\$8/LF	2000 LF	\$16,000.00
	Washed Rock	\$20/CY	75 CY	\$1,500.00
	Detention Volume	\$4.50/CY	363	\$1,633.50
			Total	\$88,311.50
			Difference	\$16,062.50



4.0 STANDARD VS. PERVIOUS ASPHALT PAVEMENT

This section compares the construction costs of Class B hot-mix asphalt pavement versus Pervious (open-graded) asphalt concrete pavement construction. The scope of this scenario is to perform research of published costs and project results and compare the cost of a typical pavement section for each pavement type. Detention and treatment volumes have been calculated and costs developed assuming a combined detention/wetpond is used for stormwater management. For this study, the pervious surfaces have been assumed to be hydrologically equivalent to grass.

The cost of pervious asphalt pavement varies considerably from source to source. Several sources stated that the cost of material and labor for the pervious asphalt is the same as standard asphalt. The difference is overall pavement cost is due to the difference in the pavement base. This cost analysis is based on that assumption. All costs are on a square foot of pavement basis.

	Item	Unit Cost	Quantity	Cost
Standard Pavement			-	
	Class B Asphalt (2")	\$35/CY	0.006 CY	\$0.21
	CSTC (2")	\$15/CY	0.006 CY	\$0.09
	Gravel Base (6")	\$12/CY	0.019 CY	\$0.23
	Treatment Volume	\$4.50/CY	0.004 CY	\$0.02
	Detention Volume	\$4.50/CY	0.020 CY	\$0.09
			Total _	\$0.64
Pervious Pavement				
	Pervious Asphalt (2")	\$35/CY	0.006 CY	\$0.21
	AASHTO Ño. 57 (2")	\$15/CY	0.006 CY	\$0.09
	AASHTO No. 3 (12")	\$18/CY	0.037 CY	\$0.66
	Treatment Volume	\$4.50/CY	0.002 CY	\$0.01
	Detention Volume	\$4.50/CY	0.007 CY	\$0.03
			Total	\$1.00
			Difference	\$0.36

5.0 RESIDENTIAL DRIVEWAY CONSTRUCTION

This section compares the costs of four construction materials for residential driveways. The five construction types are – standard asphalt pavement, pervious pavement, standard cement concrete, pervious cement concrete, eco-stone unit pavers. The standard residential driveway is assumed to be 500 square feet. Stormwater treatment and detention volumes have also been included in this cost analysis. This study assumes that pervious pavement systems are hydrologically similar to grass.



	Item	Unit Cost	Quantity	Cost
Standard Asphalt				
	Class B Asphalt (2")	\$50/CY	3 CY	\$150.00
	CSTC (4")	\$25/CY	6 CY	\$150.00
	Treatment Volume	\$4.50/CY	2 CY	\$9.00
	Detention Volume	\$4.50/CY	10 CY	\$45.00
			Total	\$354.00
D				
Pervious Asphalt	D	670 /GT	0.017	6450.00
	Pervious Asphalt (2")	\$50/CY	3 CY	\$150.00
	AASHTO No. 57 (2")	\$25/CY	3 CY	\$75.00
	AASHTO No. 3 (12")	\$25/CY	9 CY	\$225.00
	Treatment Volume	\$4.50/CY	1 CY	\$4.50
	Detention Volume	\$4.50/CY	3.5 CY	\$15.75
			Total	\$470.25
Standard Concrete				
	Cement Concrete (4")	\$155/CY	6 CY	\$930.00
	CSTC (2")	\$25/CY	3 CY	\$75.00
	Treatment Volume	\$4.50/CY	2 CY	\$9.00
	Detention Volume	\$4.50/CY	10 CY	\$45.00
			Total	\$1,059.00
Pervious Concrete				
	Pervious Concrete (4")	\$205/CY	6 CY	\$1,230.00
	AASHTO No. 57 (2")	\$25/CY	3 CY	\$75.00
	AASHTO No. 3 (12")	\$25/CY	9 CY	\$225.00
	Treatment Volume	\$4.50/CY	1 CY	\$4.50
	Detention Volume	\$4.50/CY	3.5 CY	\$15.75
			Total _	\$1,550.25
Pervious Pavers				
	Pervious Concrete (4")	\$4.50/SF	500 SF	\$2,250.00
	AASHTO No. 8 (1")	\$25/CY	1.5 CY	\$38.00
	AASHTO No. 57 (6")	\$25/CY	9 CY	\$225.00
	Treatment Volume	\$4.50/CY	1 CY	\$4.50
	Detention Volume	\$4.50/CY	3.5 CY	\$15.75
			Total _	\$2,533.25

6.0 Parking Lot Design

This analysis evaluates the construction costs for a 20,000 square foot parking lot. The analysis compares the cost of a standard asphalt parking lot with an open pond for detention/treatment, a stormwater vault for detention/treatment, and a parking lot with pervious pavement with rock gallery storage under the pavement. Two scenarios were



evaluated for the pervious options. The first assumed an infiltration rate through the native subgrade of 0.5 inches per hour while the second assumes that there is no infiltration and the system functions as a detention system. The no infiltration case would be for sites where high groundwater elevations or other site constraints preventing any infiltration through the pavement subgrade.

	Item	Unit Cost	Quantity	Cost
Impervious Parking				
(Open Pond)	Class B Asphalt (2")	\$35/CY	123 CY	\$4,305.00
	CSTC (4")	\$15/CY	246 CY	\$3,690.00
	Detention Volume	\$4.50/CY	445 CY	\$2,002.50
	Treatment Volume	\$4.50/CY	31 CY	\$139.50
	Control Structure	\$3,500/EA	1 EA	\$3,500.00
	Catch Basin	\$700/EA	2 EA	\$1,400.00
	12" CPEP Storm	\$18/LF	100 LF	\$1,800.00
	Chain Link Fence	\$7/LF	350 LF	\$2,450.00
			Total	\$19,287.00
Impervious Parking				
(Vault)	Class B Asphalt (2")	\$35/CY	123 CY	\$4,305.00
	CSTC (4")	\$15/CY	246 CY	\$3,690.00
	Detention Volume	\$3.50/CF	10,672 CF	\$37,352.00
	Treatment Volume	\$3.50/CF	828 CF	\$2,898.00
	Control Structure	3,500/EA	1 EA	\$3,500.00
	Catch Basin	\$700/EA	2 EA	\$1,400.00
	12" CPEP Storm	\$18/LF	100 LF	\$1,800.00
_			Total	\$54,945.00
Pervious Parking (Infiltration)				
(IIIIIti atioii)	Pervious Asphalt (2")	\$35/CY	123 CY	\$4,305.00
	½ Gravel (2")	\$15/CY	123 CY	\$1,845.00
	2"-4" Ballast (12")	\$18/CY	740 CY	\$13,320.00
	μ 1 Bullust (1μ)	\$107 C I	Total	\$19,470.00
Pervious Parking				, , , , , , , , , , , , , , , , , , , ,
(No Infiltration)				
	Pervious Asphalt (2")	\$35/CY	123 CY	\$4,305.00
	½ Gravel (2")	\$15/CY	123 CY	\$1,845.00
	2"-4" Ballast (18")	\$18/CY	1,111 CY	\$19,998.00
	Liner	\$1/SF	21,200 SF	\$21,200.00
	Control Structure	3,500/EA	1 EA	\$3,500.00
	12" Perf. Pipe	20/LF	400 LF	\$8,000.00
			Total	\$58,848.00



7.0 SOIL REHABILITATION

Soil rehabilitation consists of adding compost material to site soils prior to applying sod or landscaping to provide a better growth medium and provide increased stormwater retention properties. This analysis reviews the cost of this practice from a stormwater management standpoint, but there are additional benefits including reduced chemical fertilizer requirements and watering needs and increased soil biota. The soil rehabilitation costs are based on the recommended practices as outlined in Guidelines & Resources for Implementing Soil Depth & Quality, BMP T.5.13, in WDOE Western Washington Stormwater Manual, 2002 funded by Snohomish County Public Works Department. Construction cost information has been obtained from several sources including *Guidelines* for Landscaping with Compost-Amended Soils for City of Redmond Public Works prepared by Chollak Services. The Tilled Compost-Amended Turf (TCT) consists of breaking up or tilling the top 6 to 8 inches of native soil material and adding a calculated quantity of mature compost. The compost is tilled into the native material with a goal of reaching an organic content of between 8 and 13-percent for the amended soil. As stated in the referenced report, costs can vary depending on native soil conditions, availability of compost material, and size and type of equipment that can be used on a particular site.

	Item	Unit Cost	Quantity	Cost
Minimum Input Turf (MIT)				
_	Surface Preparation	\$1.00/SF	2500 SF	\$2,500.00
	Detention Volume	\$4.50/CY	6.29 CY	\$28.31
			Total	\$2,528.31
Tilled Compost-Amended				
Turf (TCT)				
	Surface Preparation	\$1.36/SF	2500 SF	\$3,400.00
	Detention Volume	\$4.50/CY	3.55 CY	\$15.98
			Total	\$3,415.98
			Differenc	\$887.67
			e	
			Per SF	\$0.36/SF

8.0 Green Roof

Green roofs are a building construction technique that includes soil and plant material in place of standard roofing systems. Green roofs typically consist of a waterproof membrane, root barrier, insulation, growth medium, and vegetation. Intensive green roofs consist of highly manicured landscape designs with turfs and shrubs. Intensive green roof also generally require irrigation and additional growth medium increasing the initial construction costs. For this project, the cost for an extensive green roof is used. Extensive green roofs consist of a thinner growth medium and the primary plant materials used are sedums which are adapted to growing in difficult conditions. This cost analysis is based on the initial construction costs and the realized savings in required stormwater management



facilities. Additional life-cycle cost savings may include reduced heating/cooling requirements, increased roof life, these not considered as part of this project. To determine stormwater management facility volume savings, the detention required for a standard roof modeled as impervious surface was compared to an extensive green roof assumed to have hydrologic characteristics comparable to grass/landscaping.

	Item	Unit Cost	Quantity	Cost
Standard Roof (Hot				
Applied Roofing)				
	Roofing	\$10.00/SF	10,000 SF	\$100,000.0
				0
	Detention Volume	\$4.50/CY	188.78 CY	\$849.51
			Total	\$100,849.51
Green Roof (Extensive)				
	Green Roof	\$12.50/SF	10,000 SF	\$125,000.0
				0
	Detention Volume	\$4.50/CY	56.48 CY	\$254.16
			Total	\$125,254.16
			Difference	\$24,404.65
			Per SF	\$2.44/SF

9.0 DETENTION FOR STANDARD RESIDENTIAL SUBDIVISION

AHBL has previously provided a case study for the Kensington Estates residential development. This study reviewed the stormwater detention and treatment requirements for a 24-acre residential subdivision located in Pierce County, Washington. Comparisons were made for multiple low impact development scenarios and were compared against a conventional development. This study is provided in Appendix G of this cost comparison.

10.0 CONCLUSION

This analysis is based on data and records either supplied to or obtained by AHBL. These documents are referenced within the text of the analysis. The analysis has been prepared using procedures and practices within the standard accepted practices of the industry.

AHBL. Inc.

Glenn C. Hume, PE Project Engineer

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APPENDIX A

WWHM Output for Infiltration Trenches vs. Bioretention Cells

WESTERN WASHINGTON HYDROLOGY MODEL V2 PROJECT REPORT

Project Name: trench

Site Address:

City

Report Date : 7/28/2004 Gage : McMillian

Data Start : 1948 Data End : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

Basin : Pre-Dev

Flows To : Point of Compliance

GroundWater: No

Land Use

TILL FOREST: 0.046

Acres

DEVELOPED LAND USE

Basin : Dev Flows To : Trench

GroundWater: No

Land Use IMPERVIOUS:

0.046

RCHRES (POND) INFORMATION

Pond Name: Trench

Pond Type:

Table

Pond Flows to : Point of Compliance Pond Rain / Evap is not activated.

Dimensions

Depth:

Oft.

Pond Hydraulic Table

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt(cfs)
35.00	0.001	0.000	0.000	0.031
35.10	0.001	0.000	0.000	0.031
35.20	0.001	0.000	0.000	σ.031
35.30	0.001	0.000	0.000	0.031
35.40	0.001	0.000	0.000	0.031
35.50	0.001	0.000	0.000	0.031
35.60	0.001	0.000	0.000	0.031
35.70	0.001	0.000	0.000	0.031
35.80	0.001	0.000	0.000	0.031
35.90	0.001	0.000	0.000	0.031
36.00	0.001	0.000	0.000	0.031
36.10	0.001	0.000	0.000	0.031
36.20	0.001	0.000	0.000	0.031
36.30	0.001	0.000	0.000	0.031
36.40	0.001	0.000	0.000	0.031
36.50	0.001	0.000	0.000	0.031
36.60	0.001	0.000	0.000	0.031
36.70	0.001	0.001	0.000	0.031
36.80	0.001	0.001	0.000	0.031
3 % UU	0 001	0 001	0 000	0 001

37.00 37.10 37.20 37.30 37.40 37.50 37.60 37.70 37.80 37.90 38.00 38.10 38.20 38.30	0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001	0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.308 0.871 1.600	0.031 0.031 0.031 0.031 0.031 0.031 0.031 0.031 0.031 0.031 0.031
38.40 38.50	0.001 0.001 0.001	0.001 0.001 0.001	1.600 2.464 3.443	0.031
	0.001	0.001	3.443	0.031

ANALYSIS RESULTS

Flow Frequency Return Return Period	Periods for Predeveloped Flow(cfs)
2 year	0.001101
5 year	0.001846
10 year	0.002405
25 year	0.003176
50 year	0.003791
100 year	0.004438

Flow Frequency Ret	urn Periods for Developed Unmitigated
Return Period	Flow(cfs)
2 year	0.014372
5 year	0.019186
10 year	0.022598
25 year	0.027174
50 year	0.030781
100 year	0.034562

Flow Frequency Return Period	Return			Developed	Mitigated
		Flow (cfs			
2 year		0.1165	71		
5 year		0.4049	98		
10 year		0.8543	347		
25 year		2.0417	29		
50 year		3.7392	259		
100 year		6.6330	62		

Yearly P	eaks for Predevelop	ed and Developed-Mitigated
Year	Fredeveloped	Developed
1949	0.002	0.000
1950	0.001	0.000
1951	0.003	0.000
1952	0.001	0.000
1953	0.001	0.000
1954	0.001	0.000
1955	0.001	0.000
1956	0.002	0.000
1957	0.001	0.000
1958	0.001	0.000
1959	0.001	0.000
1960	0.005	0.006
1961	0.001	0.000
1962	0.000	0.000
1963	0.003	0.000
1964	0.001	0.000
1965	0.001	0.000
1966	0.003	0.000
1967	0.001	0.000

1968 1969 1970 1971 1972 1973 1974 1975 1976 1977 1978 1979 1980 1981 1982 1983 1984 1985 1986 1987 1988	0.001 0.001 0.001 0.002 0.001 0.002 0.001 0.000 0.003 0.001 0.002 0.001 0.002 0.001 0.000 0.001 0.000 0.001	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1985 1986	0.001 0.001	0.000
1988	0.001	0.000
1991 1992 1993 1994 1995 1996	0.001 0.001 0.002 0.000 0.000 0.001	0.000 0.000 0.000 0.000 0.000

Ranked Yearly Peaks for Predeveloped and Developed-Mitigated Rank Predeveloped Developed

Kank	Predeveloped	Developed
1	0.0032	0.0000
2	0.0030	0.0000
3	0.0028	0.0000
4	0.0027	0.0000
5	0.0025	0.0000
6	0.0021	0.0000
7	0.0018	0.0000
8	0.0017	0.0000
9	0.0017	0.0000
10	0.0016	0.0000
11	0.0015	0.0000
12	0.0015	0.0000
13	0.0015	0.0000
14	0.0015	0.0000
15	0.0014	0.0000
16	0.0014	0.0000
17	0.0014	0.0000
18	0.0013	0.0000
19	0.0013	0.0000
20	0.0013	0.0000
21	0.0013	0.0000
22	0.0012	0.0000
23	0.0012	0.0000
24	0.0012	0.0000
25	0.0010	0.0000
26 27	0.0010	0.0000
28	0_0010	0.0000
28 29	0.0010	0.0000
30	0.0009	0.0000
31	0.0009	0.0000
32	0.0008	0.0000
33	0.0008	0.0000
34	0.0008 0.0008	0.0000
35	0.0007	0.0000
36	0.0007	0.0000
37	0.0007	0.0000
38	0.0007	0.0000 0.0000
39	0.0006	
	0.0000	0.0000

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Pass

1/2 2 year	r to 50	year	D	-
T TOW (CES)	Fredev	sinat	Percentage	Pass/Fail
0.0006	4176	2	.0	Pass
0.0006	3627	2	. 0	Pass
0.0000	21.00	~	• •	rass
0.0006	3168	2	• O	Dace

2783

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1996

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1456

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937

843

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603

543

480

432

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0.0025	10	2	20_0	Pass
0.0025	8	2	25.0	Pass
0.0026	8	2 2 2 2 2 2 2 2 2 2 2 2	25.0	Pass
0.0026	7	2	28.0	Pass
0.0026	7	2	28.0	Pass
0.0027	6	2	33.0	Pass
0.0027	5	2	40.0	Pass
0.0027	5	2	40.0	Pass
0.0028	5	2	40.0	Pass
0.0028	4	2	50.0	Pass
0.0028	3	2	66.0	Pass
0.0029	3	2	66.0	Pass
0.0029	3	2	66.0	Pass
0.0029	3	2	66.0	Pass
0.0030	3	2	66.0	Pass
0.0030	3	2	66.0	Pass
0.0030	2	2	100.0	Pass
0.0031	3° 2 2	2	100.0	Pass
0.0031	2 2	2	100.0	Pass
0.0031	2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	100.0	Pass
0.0032	2	2	100.0	Pass
0.0032	1	2	200.0	Fail
0.0032	1	2	200.0	Fall
0.0033	1	2	200.0	Fail
0.0033	1	2	200.0	Fail
0.0033	1	2	200.0	Fail
0.0034	1	2	200.0	Fail
0.0034	1	2	200.0	Fail
0.0034	1	2	200.0	Fail
0.0035	1	2	200.0	Fail
0.0035	1	2	200.0	Fail
0.0035	1	2	200.0	Fall
0.0036	1	2	200.0	Fail
0.0036	1	2	200.0	Fail
0.0036	1	2	200.0	Fail
0.0037	1	2	200.0	Fail
0.0037	1	2	200.0	Fail
0.0037	1	2	200.0	Fail
0.0038	1	2 2 2 2 2 2 2 2 2 2	200.0	Fail
0.0038	1		200.0	Fail.
The devel	opment	has an incre	ease in flow	durations

The development has an increase in flow durations from 1/2 predeveloped 2 year flow to the 2 year flow or more than a 10% increase from the 2 year to the 50 year flow.

Water Quality BMP Flow and Volume.

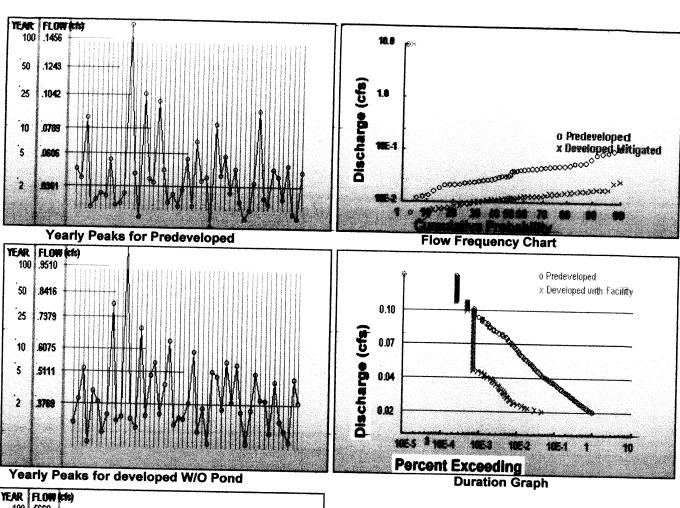
On-line facility volume: 0.138 acre-feet On-line facility target flow: 0.15 cfs.

Adjusted for 15 min: 0.17 cfs.

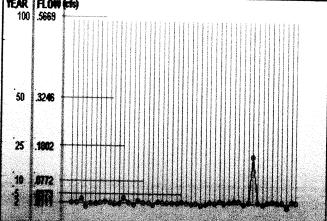
Off-line facility target flow: 0.09 cfs.

Adjusted for 15 min: 0.1 cfs.

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Yearly Peaks for Developed W/Pond

WESTERN WASHINGTON HYDROLOGY MODEL V2 PROJECT REPORT

Project Name: trench(till)

Site Address: City :

Report Date : 7/28/2004 Gage : McMillian

Data Start : 1948 **Data End** : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

Basin : Pre-Dev
Flows To : Point of Compliance
GroundWater: No

Land Use

Acres

TILL FOREST:

0.046

DEVELOPED LAND USE

Basin : Dev

Flows To : Trench(till)

GroundWater: No

Land Use

Acres

IMPERVIOUS: 0.046

RCHRES (POND) INFORMATION

Pond Name: Trench(till)
Pond Type: Table

Pond Flows to : Point of Compliance Pond Rain / Evap is not activated.

Dimensions

Depth:

Oft.

Pond Hydraulic Table

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt(cfs)
35.00	0.007	0.000	0.000	0.007
35.10	0.007	0.000	0.000	0.007
35.20	0.007	0.000	0.000	0.007
35.30	0.007	0.001	0.000	0,007
35.40	0.007	0.001	0.000	0.007
35.50	0.007	0.001	0.000	0.007
35.60	0.007	0.001	0.000	0.007
35.70	0.007	0.001	0.000	0.007
35.80	0.007	0.002	0.000	0.007
35-90	0.007	0-002	0-000	0.007
36.00	0.007	0.002	0.000	0.007
36.10	0.007	0.002	0.000	0.007
36.20	0.007	0.002	0.000	0.007
36.30	0.007	0.003	0.000	0.007
36.40	0.007	0.003	0.000	0.007
36.50	0.007	0.003	0.000	0.007
36.60	0.007	0.003	0.000	0.007
36.70	0.007	0.004	0.000	0.007
36.80	0.007	0.004	0.000	0.007

37.00 0.007 37.10 0.007 37.20 0.007 37.30 0.007 37.40 0.007 37.50 0.007 37.70 0.007 37.80 0.007 37.90 0.007 38.10 0.007 38.20 0.007 38.30 0.007 38.40 0.007 38.50 0.007	0.004 0.004 0.005 0.005 0.005 0.005 0.006 0.006 0.006 0.006 0.006 0.007	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.308 0.871 1.600 2.464 3.443	0.007 0.007 0.007 0.007 0.007 0.007 0.007 0.007 0.007 0.007 0.007
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ANALYSIS RESULTS

Flow	Frequency	Return	Periods	for	Predeveloped
	n Period		Flow(cfs		7

	TTON (CTS)
2 year	0.001101
5 year	0.001846
10 year	0.002405
25 year	0.003176
50 year	0.003791
100 year	0.004438

Flow Frequency Return Periods for Developed Unmitigated

Return Period	Flow(cfs)		
2 year	0.014372		
5 year	0.019186		
10 year	0.022598		
25 year	0.027174		
50 year	0.030781		
100 year	0.034562		

Flow Frequency Return Periods for Developed Mitigated

Return Period	Flow(cfs)		
2 year	0.008358		
5 year	0.046501		
10 year	0.130081		
25 year	0.432149		
50 year	0.994897		
100 year	2.191918		

Yearly Peaks for Predeveloped and Developed-Mitigated Year Predeveloped Developed

Tear	bredeverobed.	neverobe
1949	0.002	0.000
1950	0.001	0.000
1951	0.003	0.000
1952	0.001	0.000
1953	0.001	0.000
1954	0.001	0.000
1955	0.001	0_000
1956	0.002	0.000
1957	0.001	0.000
1958	0.001	0.000
1959	0.001	0.000
1960	0.005	0.000
1961	0.001	0.000
1962	0.000	0.000
1963	0.003	0.000
1964	0.001	0.000
1965	0.001	0.000
1966	0.003	0.000
1967	0.001	0.000

1968 1969 1970 1971 1972 1973 1974 1975 1976 1977 1978 1979 1980 1981 1982 1983 1984 1985 1986 1987	0.001 0.001 0.001 0.001 0.002 0.001 0.002 0.001 0.000 0.003 0.001 0.002 0.001 0.002 0.001 0.002 0.001 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
	•	
1982	0.002	
	0.001	0.000
		0.000
1988	0.003	
1989	0.001	0.000 0.000
1990	0.001	0.000
1991	0.001	0.000
1992	0.001	0.000
1993	0.002	0.900
1994 1995	0.000	0.000
1996	0.000 0.001	0.000
±230	0.001	0.000

Ranked	Yearly Peaks for	Predeveloped and Developed-Mitigated
Rank	Predeveloped	Developed
1	0.0032	0.0000
2	0.0030	0.0000
3	0.0028	0.0000
4	0.0027	0.0000
5	00025	0.0000
6	0.0021	0.0000
7	0.0018	0.0000
8	0.0017	0.0000
9	0.0017	0,0000
10	0.0016	0.0000
11	0.0015	0.0000
12	0.0015	0.0000
13	0.0015	0.0000
14	0.0015	0.0000
15	0.0014	0.0000
16	0.0014	0.0000
17	0.0014	0.0000
18	0.0013	0.0000
19	0.0013	0.0000
20"	0.0013	0.0000
21	0.0013	0.0000
22	0.0012	0.0000
23	0.0012	0.0000
24	0.0012	0.0000
25	0.0010	0.0000
26	0.0010	0.0000
27	0-0010	0_0000
28	0.0010	0.0000
29	0.0009	0.0000
30 31	0.0009	0.0000
	0.0008	0.0000
32	0.0008	0.0000
33 34	0.0008	0.0000
34 35	0.0008	0.0000
36	0.0007 0.0007	0.0000
37	0.0007	0.0000
38	0.0007	0.0000
39	0.0007	0.0000
J 3	0.0000	0.0000

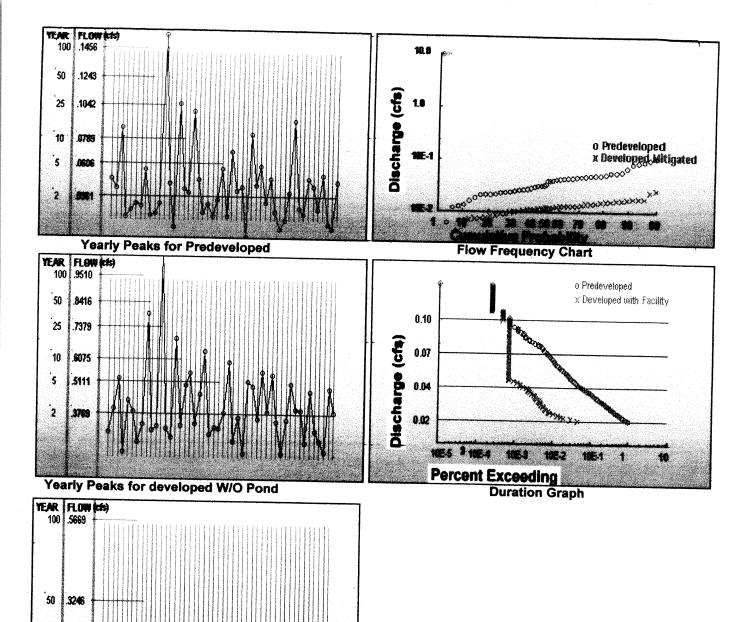
46 47	0.0004		0.000	0
Flow (CFS 0.0006 0.0006 0.0006 0.0007 0.0007 0.0007	4176 3627 3168 2783 2464 2200 1996	Final 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Percentage .0 .0 .0 .0 .0 .0 .0 .0	Pass Pass Pass Pass Pass Pass Pass
0.0008 0.0008 0.0009 0.0009 0.0009 0.0010 0.0010 0.0011 0.0011	1807 1620 1456 1313 1175 1054 937 843 746 667 603 543	0 0 0 0 0 0 0	.0	Pass Pass Pass Pass Pass Pass Pass Pass
0.0012 0.0012 0.0012 0.0013 0.0013 0.0014 0.0014 0.0014 0.0015 0.0015	480 432 378 332 293 261 236 210 184 171 158	0 0 0 0 0 0 0 0	.0 .0 .0 .0 .0 .0	Pass Pass Pass Pass Pass Pass Pass Pass
0.0015 0.0016 0.0016 0.0017 0.0017 0.0017 0.0018 0.0018	143 129 120 114 105 95 89 80 71 65	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.0	Pass Pass Pass Pass Pass Pass Pass Pass
0.0019 0.0019 0.0019 0.0020 0.0020 0.0021 0.0021 0.0021 0.0022	60 56 50 47 46 42 39 36 34 31 29	0 0 0 0 0 0 0	.0	Pass Pass Pass Pass Pass Pass Pass Pass
0.0022 0.0023 0.0023 0.0023 0.0024 0.0024 0.0024 0.0024 0.0025	26 24 23 22. 18 17 14 12	0 0 0 0 0 0 0	.0	Pass Pass Pass Pass Pass Pass Pass Pass

Water Quality BMP Flow and Volume.

On-line facility volume: 0.138 acre-feet On-line facility target flow: 0.15 cfs. Adjusted for 15 min: 0.17 cfs. Off-line facility target flow: 0.09 cfs.

Adjusted for 15 min: 0.1 cfs.

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25 .1002

Yearly Peaks for Developed W/Pond

WESTERN WASHINGTON HYDROLOGY MODEL V2 PROJECT REPORT

Project Name: roof drain

Site Address:

City :

Report Date : 7/27/2004 Gage : McMillian Data Start : 1948 **Data End** : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

Basin : Pre-Dev
Flows To : Point of Compliance

GroundWater: No

Land Use Acres TILL FOREST: 0.046

DEVELOPED LAND USE Basin : Dev Flows To : Pond 1 GroundWater: No

Land Use Acres IMPERVIOUS: 0.046

RCHRES (POND) INFORMATION

Pond Name: Pond 1
Pond Type: Trapezoidal Pond Pond Flows to : Point of Compliance

Pond Rain / Evap is activated.

Dimensions

Depth: 1ft. Bottom Length: 45ft. Bottom Width: 10ft. Side slope 1: 3 To 1 Side slope 2: 3 To 1 Side slope 3: 3 To 1 Side slope 4: 3 To 1

Volume at Riser Head: 0.006 acre-ft.

Discharge Structure Riser Height: 0.5 ft. Riser Diameter: 12 in.

Pond Hydraulic Table

Stage (ft)	Area (acr)	Volume (acr-ft)	Dachrg (cfs)	Infilt(cfs)
0.000	0.010	0.000	0.000	0.000
0.044	0.011	0.000	0.000	0.011
0.089	0.011	0.001	0.000	0.011
0.133	0.011	0.001	0.000	0.012
0.178	0.012	0.002	0.000	0.012
0.222	0.012	0.002	0.000	0.012
0.267	0.012	0.003	0.000	0.013
0.311	0.013	0.004	0.000	0.013
0.356	0.013	0.004	0.000	0.013

0.400 0.444 0.489 0.533 0.578 0.622 0.667 0.711 0.756 0.800 0.844	0.013 0.014 0.014 0.015 0.015 0.015 0.016 0.016 0.017 0.017	0.005 0.005 0.006 0.007 0.007 0.008 0.009 0.009 0.010 0.011	0.000 0.000 0.000 0.059 0.211 0.416 0.663 0.945 1.258 1.600 1.969	0.014 0.014 0.015 0.015 0.015 0.016 0.016 0.017 0.017 0.017
0.756 0.800	0.017 0.017	0.010 0.011	1.258 1.600	0.017 0.017
0.978 1.022	0.019	0.014	3.216 3.675	0.019

ANALYSIS RESULTS

Flow Frequency Retu	urn Periods for Predeveloped
Return Period	Flow(cfs)
2 year	0.001101
5 year	0.001846
10 year	0.002405
25 year	0.003176
50 year	0.003791
100 year	0.004438

Flow Frequency	Return	Periods for	Developed	Unmitigated
Return Period		Flow(cfs)	-	
2 year		0.014372		
5 year		0.019186		
10 year		0.022598		
25 year		0.027174		
50 year		0.030781		
100 year		0.034562		

Flow Frequency Ret	urn Periods for Developed Mitigated
Return Period	Flow(cfs)
2 year	0.00757
5 year	0.010085
10 year	0.01194
25 year	0.014508
50 year	0.016591
100 year	0.018825

Yearly	Peaks for Predev	eloped and Developed-N
Year	Predevelop	
1949	0.002	0.000
1950	0.001	Q.000
1951	0.003	0.000
1952	0.001	0.000
1953	0.001	0.000
1954	0.001	0.000
1955	0.001	0_000
1956	0.002	0.000
1957	0.001	0.000
1958	0.001	0.000
1959	0.001	0.000
1960	0.005	0.000
1961	0.001	0.000
1962	0.000	0.000
1963	0.003	0.000
1964	0.001	0.000
1965	0.001	0.000
1966	0.003	0.000
1967	0.001	0.000
4 0 0 0	0 001	0 000

Ranked Yearly Peaks for Predeveloped and Developed-Mitigated Rank Predeveloped Developed

Rank	Predeveloped	Develope
1	0.0032	0.0000
2	0.0030	0.0000
3	0.0028	0.0000
4	0.0027	0.0000
5	0.0025	0.0000
6	0.0021	0.0000
7	0.0018	0.0000
8	0.0017	0.0000
9	0.0017	0.0000
10	0.0016	0.0000
11	0.0015	0.0000
12	0.0015	0.0000
13	0.0015	0.0000
14	0.0015	Q.0000
15	0.0014	0.0000
16	0.0014	0.0000
17	0.0014	0.0000
18	0.0013	0.0000
19	0.0013	0.0000
20	0.0013	0.0000
21	0_0013	0.0000
22	0.0012	0.0000
23 2 4	0.0012	0.0000
24 25	0.0012	0.0000
26	0.0010 0.0010	0.0000
27	0.0010	0.0000
28	0.0010	0.0000 0.0000
29	0.0009	0.0000
30	0.0009	0.0000
31	0.0008	0.0000
32	0.0008	0.0000
33	0.0008	0.0000
34	0.0008	0.0000
35	0.0007	0.0000
36	0.0007	0.0000
37	0.0007	0.0000
38	0.0007	0.0000
39	0.0006	0.0000
40	0 0006	0 0000

41	0.0006	0.0000
42	0.0006	0.0000
43	0.0005	0.0000
44	0.0004	0.0000
45	0.0004	0.0000
46	0.0004	0.0000
47	0.0002	0.0000

1/2 2 yea	r to 50	Wear.		
Flow (CFS)		Final	Percentage	Pass/Fail
0.0006	4176	0	.0	Pass
0.0006	3627	0	.0	Pass
0.0006	3168	0	.0	Pass
0.0006	2783	0	.0	Pass
0.0007	2464 2200	0	_0	Pass
0.0007	1996	0 0	.0 .0	Pass
0.0008	1807	0	.0	Pass Pass
0.0008	1620	Ö	.0	Pass
0.0008	1456	0	.0	Pass
0.0009	1313	0	.0	Pass
0.0009	1175	0	.0	P as s
0.0009 0.0010	1054 937	0 0	.0 .0	Pass
0.0010	843	0	.0	Pass Pass
0.0010	746	Ö	.0	Pass
0.0011	667	0	.0	Pass
0.0011	603	0	.0	Pass
0.0011	543	0	.0	Pass
0.0012	480	0	.0	Pass
0.0012	432 378	0 0	.0 .0	Pass
0.0012	332	0	.0	Pass Pass
0.0013	293	Ö	.0	Pass
0.0013	261	0	.0	Pass
0.0014	236	0	.0	Pass
0-0014	210	0	_0 .	Pass
0.0014	184	0	.0	Pass
0.0015 0.0015	171 158	0	.0	Pass
0.0015	143	0 0	.0	Pass
0.0016	129	0	.0	Páss Pass
0.0016	120	Ö	.0	Pass
0.0016	114	0	.0	Pass
0.0017	105	0	.0	Pass
0.0017	95	0	.0	Pass
0.0017	89	0	.0	Pass
0.0018 0.0018	80 71	0 0	.0	Pass
0.0018	65	0	.0 .0	Pass Pass
0.0019	60	Ö	.0	Pass
0.0019	56	0.	.0	Pass
0.0019	50	0	.0	Pass
0.0020	47	0	.0	Pass
0.0020	46	0	.0	Pass
0.0020 0.0021	42 39	0 0	.0	Pass
0.0021	36	0	.0	Pass Pass
0-0021	34	0	-a	Pass
0.0022	31	0	.0	Pass
0.0022	29	0	.0	Pass
0.0022	26	0	.0	Pass
0.0023	24	0	.0	Pass
0.0023 0.0023	23 22	0 0	.0	Pass
0.0023	18	0	.0	Pass Pass
0.0024	17	0	.0	Pass
0.0024	14	Ö	.0	Pass
0.0024	12	0	.0	Pass
0.0025	10	0	.0	Pass
0.0025	10	0	.0	Pass

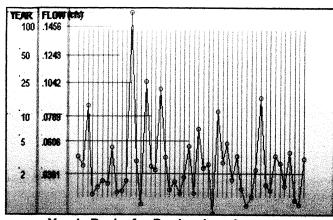
Water Quality BMP Flow and Volume.

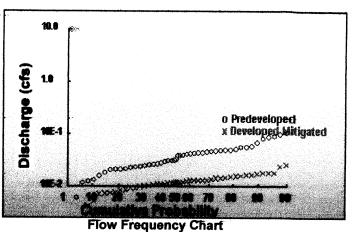
On-line facility volume: 0.109 acre-feet On-line facility target flow: 0.11 cfs. Adjusted for 15 min: 0.11 cfs.

Off-line facility target flow: 0.06 cfs.

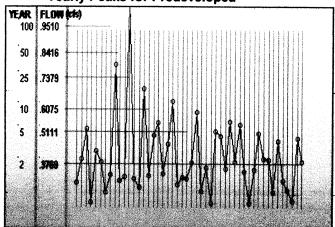
Adjusted for 15 min: 0.06 cfs.

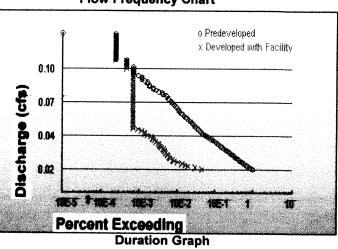
program and accompanying documentation as provided 'as-is' without warranty of any kind. The entire risk regarding the performance and results of this program is assumed by the user. AQUA TERRA Consultants and the Washington State Department of Ecology disclaims all warranties, either expressed or implied, including but not limited to implied warranties of program and accompanying documentation. In no event shall AQUA TERRA Consultants and/or the Washington State Department of Ecology be liable for any damages whatsoever (including without limitation to damages for loss of business profits, loss of business information, business interruption, and the like) arising out of the user of, or inability to use this program even if AQUA TERRA Consultants or the Washington State Department of Ecology has been advised of the possibility of such damages.



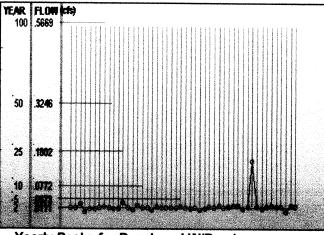


Yearly Peaks for Predeveloped





Yearly Peaks for developed W/O Pond



Yearly Peaks for Developed W/Pond

WESTERN WASHINGTON HYDROLOGY MODEL V2 PROJECT REPORT

Project Name: driveway(trench)

Site Address:

City :

Report Date : 7/28/2004 Gage : McMillian

Data Start : 1948 Data End : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

Basin : Pre-Dev
Flows To : Point of Compliance

GroundWater: No

Land Use

TILL FOREST:

0.011

DEVELOPED LAND USE

Basin : Dev
Flows To : Trench(driveway)

GroundWater: No

Land Use

Acres

IMPERVIOUS:

0.011

RCHRES (POND) INFORMATION

Pond Name: Trench(driveway)
Pond Type: Table

Pond Flows to : Point of Compliance

Pond Rain / Evap is activated.

Dimensions

Depth:

Oft.

Pond Hydraulic Table

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt(cfs)
35.00	0.000	0.000	0.000	0.010
35.10	0.000	0.000	0.000	0.010
35.20	0.000	0.000	0.000	0.010
35.30	0.000	0.000	0.000	0.010
35.40	0.000	0.000	0.000	0.010
35.50	0.000	0.000	0.000	0_010
35.60	0.000	0.000	0.000	0.010
35.70	0.000	0.000	0.000	0.010
35.80	0.000	0.000	0.000	0.010
35.90	0.000	0.000	0.000	0.010
36.00	0.000	0.000	0.000	0.010
36.10	0.000	0.000	0.000	0.010
36.20	0.000	0.000	0.000	0.010
36.30	0.000	0.000	0.000	0.010
36.40	0.000	0.000	0.000	0.010
36.50	0.000	0.000	0.000	0.010
36.60	0.000	0.000	0.000	0.010
36.70	0.000	0.000	0.000	0-010
36.80	0.000	0.000	0.000	0.010
26.00	2 222	^ ^^^	^ ^^^	0 010

	37.00 37.10 37.20 37.30 37.40 37.50 37.60 37.70 37.80 37.90 38.00 38.10 38.20 38.30 38.30 38.40	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.308 0.871 1.600 2.464 3.443	0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010
--	--	--	--	--	--

ANALYSIS RESULTS

Flow Frequency Return	Periods for Predeveloped
Return Period	Flow(cfs)
2 year	0.001101
5 year	0.001846
10 year	0.002405
25 year	0.003176
50 year	0.003791
100 year	0.004438

Flow Frequency	Return	Periods for	Developed	Unmitigated
Return Period		Flow(cfs)	_	•
2 year		0.002874		
5 year		0.003837		
10 year		0.00452		
25 year		0.005435		
50 year		0.006156		
100 year		0.006912		

Flow Frequency	Return	Periods :	for	Developed	Mitigated
Return Period		Flow (cfs		-	J
2 year		0.0173	31		
5 year		0.0276	32		
10 year		0.0354	45		
25 year		0.0464	09		
50 year		0.0553	55		
100 year		0.0649	62		

Yearly	Peaks	for Predevelop	ed and Deve
Year		Predeveloped	Developed
1949		0.000	0.000
1950		0.000	0.000
1951		0.001	0.000
1952		0.000	0.000
1953		0.000	0.000
1954		0.000	0.000
1955		0.000	0_000
1956		0.000	0.000
1957		0.000	0.000
1958		0.000	0.000
1959		0.000	0.000
1960		0.001	0.000
1961		0.000	0.000
1962		0.000	0.000
1963		0.001	Q.000
L964		0.000	0.000
1965		0.000	0.000
1966		0.001	0.000
1967		0 000	0 000

1968 1969 1970 1971 1972 1973 1974 1975 1976 1977 1978 1979 1980 1981 1982 1983 1984 1985	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
-		
1980		
1981	0.000	0.000
1982	0.000	0.000
	0.000	0.000
		0.000
,		0.000
	0.000	0.000
1987	0.001	0.000
1988	0.000	0.000
1989 1990	0.000	0.000
1991	0.000	0.000
1992	0.000	0.000
1993	0.000	0.000
1994	0.000	0.000
1995	0.000	0.000
1996	0.000	0.000

Ranked Yearly Peaks for Predeveloped and Developed-Mitigated Rank Predeveloped Developed

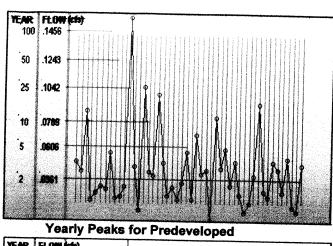
Rank	Predeveloped	Develope
1	0.0006	0.0000
2	0.0006	0.0000
3	0.0006	0.0000
4	0.0005	0.0000
5	00005	0.0000
6	0.0004	0.0000
7	0.0004	0.0000
8	0.0003	0.0000
9	0.0003	0.0000
10	0.0003	0.0000
11	0.0003	0.0000
12	0.0003	0.0000
13	0.0003	0.0000
14	0.0003	0.0000
15	0.0003	0,0000
16	0.0003	0.0000
17	0.0003	0.0000
18	0.0003	0.0000
19	0.0003	0.0000
20	0.0003	0-0000
21	0.0003	0.0000
22	0.0002	0.0000
23	0.0002	0.0000
24	0.0002	0.0000
25	0.0002	0.0000
26	0.0002	0.0000
27	0.0002	0.0000
28	0.0002	0.0000
29	0.0002	0.0000
30	0.0002	0.0000
31	0.0002	0.0000
32	0.0002	0.0000
33 34	0.0002	0.0000
35	0.0002	0.0000
	0.0001	0.000
36 37	0.0001	0.0000
38	0.0001	0.0000
39	0.0001	0.0000
שנ	0.0001	0.0000

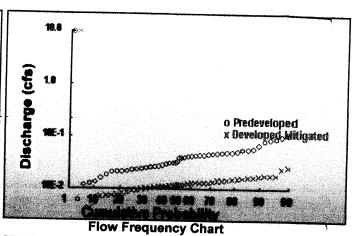
40	0.0001 0.0001	0.0000
42	0.0001	0.0000
43	0.0001	0.0000
44	0.0001	0.0000
45	0.0001	0.0000
46	0.0001	0.0000
47	0.0000	0.0000

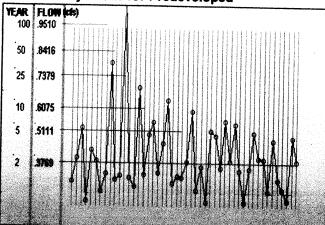
1/2 2 yea	r to 50	year		
Flow (CFS)			Percentage	Pass/Fail
0.0006	5	0	.0	Pass
0.0006	3	0	.0	Pass
0.0006	2	0	.0	Pass
0.0006	1	0.	.0"	Pass
0.0007	1	0	.0	Pass
0.0007	1	0	.0	Pass
0.0007	1	0	.0	Pass
0.0008	1	0	.0	Pass
0.0008	1	0	.0	Pass
0.0008	1	0	.0	Pass
0.0009	1. 1	0	-O.	Pass
0.0009 0.0009	1	0 0	.0 .0	Pass
0.0010	0	0	.0	Pass
0.0010	0	0	.0	P ass Pass
0.0010	0	0	.0	Pass
0.0011	Ö	0	.0	Pass
0.0011	0	Ö	.0	Pass
0.0011	Ō	Ö	.0	Pass
0.0012	Ō	Ö	.0	Pass
0.0012	Ō	Õ	.0	Pass
0.0012	0	0	.0	Pass
0.0013	0	0	.0	Pass
0.0013	0	0	.0	Pass
0.0013	0	0	.0	Pass
0.0014	0.	0.	.0	Pass
0.0014	0	0	.0	Pass
0.0014	0	0	.0	Pass
0.0015	0	0	.0	Pass
0.0015	0	0	.0	Pass
0.0015	0	0	.0	Pass
0.0016	0	0	.0	Pass
0.0016	0	0	-0	Pass
0.0016 0.0017	0	0	.0	Pass
0.0017	0	0	.0	Pass
0.0017	0	0	.0	Pass
0.0017	0	0	.0	Pass
0.0018	0	0	.0	Pass
0.0018	0	0	.0	Pass Pass
0.0019	0	0	.0	Pass
0.0019	Ö	Ö	.0	Pass
0.0019	0	Ö	.0	Pass
0.0020	0	Ō	.0	Pass
0.0020	0	0	.0	Pass
0.0020	0	0	.0	Pass
0.0021	0	0	.0	Pass
0.0021	0,	0.	_0°	Pass
0.0021	0	0	.0	Pass
0.0022	0	0	.0	Pass
0.0022	0	0	.0	Pass
0.0022	0	0	.0	Pass
0.0023	0	0	.0	Pass
0.0023	0	0	.0	Pass
0.0023	0	0	-0-	Pass
0.0024 0.0024	0	0	.0	Pass
0.0024	0	0 0	.0	Pass
0.0024	0	0	.0	Pass
0.0025	0	0	.0	Pass
0.0023	V	v	• 0	Pass

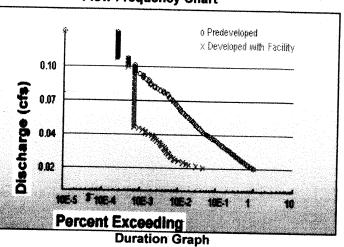
On-line facility volume: 0.109 acre-feet On-line facility target flow: 0.11 cfs. Adjusted for 15 min: 0.11 cfs. Off-line facility target flow: 0.06 cfs.

Adjusted for 15 min: 0.06 cfs.

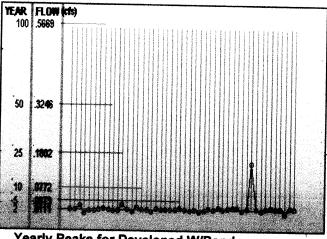








Yearly Peaks for developed W/O Pond



Yearly Peaks for Developed W/Pond

Project Name: driveway

Site Address:

City :

Report Date : 7/28/2004 Gage : McMillian

Data Start : 1948 Data End : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

Basin : Pre-Dev
Flows To : Point of Compliance

GroundWater: No

Land Use

TILL FOREST:

0.011

DEVELOPED LAND USE Basin : Dev Flows To : Pond 1

GroundWater: No

Land Use

Acres

IMPERVIOUS:

0.011

RCHRES (POND) INFORMATION

Pond Name: Pond 1
Pond Type: Trapezoidal Pond

Pond Flows to : Point of Compliance

Pond Rain / Evap is activated.

Dimensions

Depth: 1ft. Bottom Length: 15ft.
Bottom Width: 4.5ft.
Side slope 1: 3 To 1
Side slope 2: 3 To 1
Side slope 3: 3 To 1 Side slope 4: 3 To 1

Volume at Riser Head: 0.001 acre-ft.

Discharge Structure Riser Height: 0.5 ft. Riser Diameter: 12 in.

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt (ofs)
0.000	0.002	0.000	0.000	0.000
0.044	0.002	0.000	0.000	0.002
0.089	0.002	0.000	0.000	0.002
0.133	0.002	0.000	0,000	0.002
0.178	0.002	0.000	0.000	0.002
0.222	0.002	0.000	0.000	0.002
0.267	0.002	0.001	0.000	0.002
0.311	0.002	0.001	0.000	0.003
0.356	0.003	0.001	0.000	0.003

0.444 0.003 0.001 0.000 0 0.489 0.003 0.001 0.000 0 0.533 0.003 0.001 0.059 0 0.578 0.003 0.001 0.211 0 0.622 0.004 0.002 0.416 0 0.667 0.004 0.002 0.663 0 0.711 0.004 0.002 0.945 0 0.756 0.004 0.002 1.258 0 0.800 0.004 0.002 1.600 0 0.844 0.004 0.002 1.969 0 0.889 0.005 0.003 2.362 0 0.978 0.005 0.003 3.216 0	0.003 0.003 0.003 0.004 0.004 0.004 0.004 0.004 0.005 0.005
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Flow Frequency Retur	n Periods for Predeveloped
Return Period	Flow(cfs)
2 year	0.001101
5 year	0.001846
10 year	0.002405
25 year	0.003176
50 year	0.003791
100 year	0.004438

Flow Frequency	Return	Periods for Developed Unmitigated
Return Period		Flow(cfs)
2 year		0.002874
5 year		0.003837
10 year		0.00452
25 year		0.005435
50 year		0.006156
100 year		0.006912

Flow Frequency Return Period	Return	Periods for Flow(cfs)	Developed	Mitigated
2 year		0.00757		
5 year		0.010085		
10 year		0.01194		
25 year		0.014508		
50 year		0.016591		
100 year		0.018825		

			
Yearly	Peaks	for Predevelop	ed and Deve
Year		Predeveloped	Developed
1949		0.000	0.000
1950		0.000	0.000
1951		0.001	0.000
1952		0.000	0.000
1953		0.000	0.000
1954		0.000	0.000
1955		0.000	0.000
1956		0.000	0.000
1957		0.000	0.000
1958		0.000	0.000
1959		0.000	0.000
1960		0.001	0.000
1961		0.000	0.000
1962		0.000	0.000
1963		0.001	0.000
1964		0.000	0.000
1965		0.000	0.000
1966		0.001	0.000
1967		0.000	0.000
1968		0 000	0 000

1969 1970 1971 1972 1973 1974 1975 1976 1977 1978	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.001	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1980 1981	0.000	0.000
1982 1983	0.000	0.000
1984 1985 1986	0.000	0.000
1987 1988	0.000 0.001 0.000	0.000
1989 1990	0.000	0.000
1991 1992 1993	0.000 0.000	0.000
1994 1995	0.000	0.000 0.000 0.000
1996	0.000	0.000

Ranked Yearly Peaks for Predeveloped and Developed-Mitigated Rank Predeveloped Developed

Rank	Predeveloped	Developed
1	0.0006	0.0000
2	0.0006	0.0000
3	0.0006	0.0000
4	0.0005	0.0000
5	0.0005	0.0000
6	0.0004	0.0000
7	0.0004	0.0000
8	0.0003	0.0000
9	0.0003	0.0000
10	0.0003	0.0000
11	0.0003	0.0000
12	0.0003	0.0000
13	0.0003	0.0000
14	0.0003	0.0000
15	0.0003	0.0000
16	0.0003	0.0000
17	0.0003	0.0000
18	0.0003	0.0000
19	0.0003	0.0000
20	0.0003	0.0000
21:	0.0003	0.0000
22	0.0002	0.0000
23	0.0002	0.0000
24	0.0002	0.0000
25	0.0002	0.0000
26	0.0002	0.0000
27	0.0002	0.0000
28	0.0002	0.0000
29	0.0002	0.0000
30	0.0002	0.0000
31 32	0.0002	0.0000
33	0.0002	0.0000
33 34	0.0002	0.0000
35 35	0.0002	0.0000
	0.0001	0.0000
36 37	0.0001	0.0000
38	0.0001	0.0000
39	0.0001	0.0000
40	0.0001	0.0000
4 ()	0.0001	0.0000

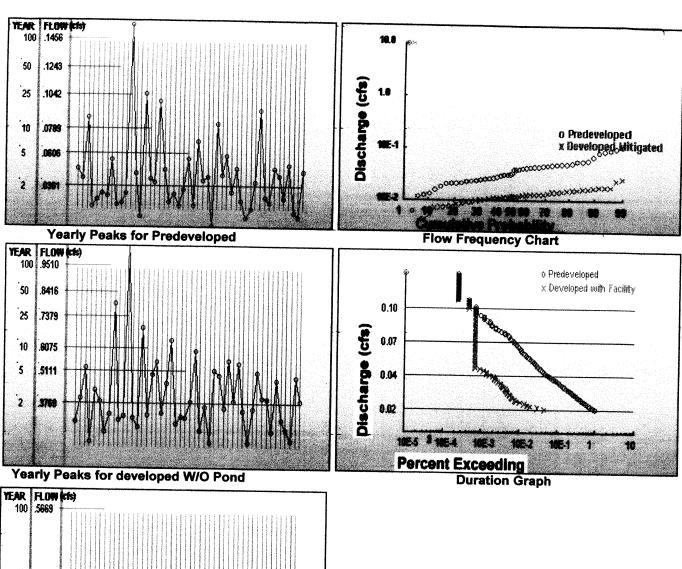
41	0.0001	0.0000
42	0.0001	0.0000
43	0.0001	0.0000
44	0.0001	0.0000
45	0.0001	0.0000
46	0.0001	0.0000
47	0.0000	0.0000

1/2 2 yea:	r +o 50	****		
Flow (CFS)			D	
•	Predev		Percentage	
0.0006	5	0	.0	Pass
0.0006	3	0	.0	Pass
0.0006	2	0	.0	Pass
0.0006	1	0	.0	Pass
0-0007	1	0	-0	Pass
0.0007	1	0	.0	Pass
0.0007	1	0	.0	Pass
0.0008	1	0	.0	Pass
0.0008	1	0	.0	Pass
0.0008	1	0	.0	Pass
0.0009	1	0	.0	Pass
0.0009	1	0	.0	Pass
0.0009	1	0	.0	Pass
0.0010	0	0	.0	Pass
0.0010	0	0	.0	Pass
0.0010	0	0	.0	Pass
0.0011	0	0	.0	Pass
0.0011	0	0	.0	Pass
0.0011	0	0	.0	Pass
0.0012	0.	0.	.o°	Pass
0.0012	Ö	Ö	.0	Pass
0.0012	Ö	0	.0	
0.0013	0	0	.0	Pass
0.0013	0	0	.0	Pass
0.0013	0	0		Pass
0.0013			.0	Pass
0.0014	0	0	.0	Pass
	0	0	ـم	Pass
0.0014	0	0	.0	Pass
0.0015	0	0	.0	Pass
0.0015	0	0	.0	Pass
0.0015	0	0	.0	Páss
0.0016	0	0	.0	Pass
0.0016	0	0	.0	Pass
0.0016	0	0	.0	Pass
0.0017	0	0	.0	Pass
0.0017	0	0	.0	Pass
0.0017	0	0	.0	Pass
0.0018	0	0	.0	Pass
0.0018	0	0	.0	Pass
0.0018	0	0	.0	Pass
0.0019	0	0	.0	Pass
0.0019	0 .	0.	.0	Pass
0.0019	0	0	.0	Pass
0.0020	0	0	.0	Pass
0.0020	0	0	.0	Pass
0.0020	0	Ō	.0	Pass
0.0021	0	Ö	.0	Pass
0.0021	0	Ö	.0	Pass
0.0021	û.	Ö.	-0.	Pass
0.0022	0	0	.0	
0.0022	0	0	.0	Pass
0.0022	0	0		Pass
			.0	Pass
0.0023	0	0	.0	Páss
0.0023	0	0	.0	Pass
	0	0	.0	Pass
	0	0	.0	Pass
	0	0	.0	Pass
	0	0	.0	Pass
	0	0	.0	Pass
	0	0	.0	Pass
0.0025	0	0	.0	Pass

0.0025 0.0026 0.0026 0.0027 0.0027 0.0027 0.0028 0.0028 0.0029 0.0029 0.0029 0.0030 0.0031 0.0031 0.0031 0.0032 0.0032 0.0032 0.0033 0.0033 0.0033 0.0035 0.0035 0.0035 0.0035 0.0036 0.0036 0.0037 0.0037 0.0038 0.0038	000000000000000000000000000000000000000			Pass Pass Pass Pass Pass Pass Pass Pass
--	---	--	--	--

On-line facility volume: 0.109 acre-feet On-line facility target flow: 0.11 cfs. Adjusted for 15 min: 0.11 cfs. Off-line facility target flow: 0.06 cfs.

Adjusted for 15 min: 0.06 cfs.



50 3246

Yearly Peaks for Developed W/Pond

APPENDIX B

WWHM Output for 24' Standard Road vs. LID Road Section

Project Name: 24' standard road

Site Address:

City

Report Date : 6/9/2004 Gage : McMillian

Data Start : 1948 Data End : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

: Pre-Dev

Flows To : Point of Compliance

GroundWater: No

Land Use

TILL FOREST:

DEVELOPED LAND USE

: Dev

Flows To : Pond 1 GroundWater: No

Land Use

TILL GRASS:

Acres 0.492

IMPERVIOUS:

1.148

RCHRES (POND) INFORMATION

Pond Name: Pond 1
Pond Type: Trapezoidal Pond

Pond Flows to : Point of Compliance Pond Rain / Evap is not activated.

Dimensions

Depth:

4ft.

Bottom Length: 148.2ft. Bottom Width: 49.41ft. Side slope 1: 3 To 1

Side slope 2: 3 To 1 Side slope 3: 3 To 1

Side slope 4: 3 To 1

Volume at Riser Head: 0.634 acre-ft. 27617 CF -> 1023 04

Discharge Structure Riser Height: 3 ft. Riser Diameter: 18 in. NotchType : Rectangular Notch Width : 0.018 ft. Notch Height: 1.155 ft.

Orifice 1 Diameter: 0.71104 in. Elevation: 0 ft.

Stag	e (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt(cfs)
0.00	0	0.168	0.000	0.000	0.000
0.04	4	0.169	0.007	0.003	0.000
0.08	9	0.171	0.015	0.004	0.000
0.13	3	0.172	0.023	0.005	0.000

0.178 0.173 0.222 0.174 0.267 0.175 0.311 0.177 0.356 0.178 0.400 0.179 0.444 0.180 0.489 0.182 0.533 0.183 0.578 0.184 0.622 0.185 0.667 0.187 0.711 0.188 0.756 0.189 0.800 0.190 0.844 0.192 0.889 0.193 0.978 0.196 1.022 0.197 1.067 0.198 1.111 0.199 1.200 0.202 1.244 0.203 1.289 0.205 1.333 0.206 1.378 0.207 1.422 0.208 1.467 0.210 1.511 0.211 1.556 0.212 1.600 0.214 1.644 0.215 1.689 0.216 1.
0.030 0.038 0.046 0.054 0.062 0.069 0.077 0.085 0.094 0.102 0.110 0.118 0.127 0.135 0.143 0.152 0.160 0.169 0.178 0.186 0.195 0.204 0.213 0.222 0.231 0.240 0.249 0.258 0.267 0.277 0.286 0.295 0.305 0.314 0.324 0.324 0.334 0.343 0.353 0.363
0.006 0.006 0.007 0.007 0.008 0.008 0.009 0.009 0.010 0.010 0.011 0.011 0.012 0.012 0.012 0.013 0.013 0.013 0.013 0.013 0.014 0.014 0.014 0.015 0.015 0.015 0.015 0.016 0.016 0.016 0.016 0.016 0.017 0.017 0.017 0.017 0.017 0.017 0.018 0.018 0.019
0.000 0.000

3.378 3.422 3.467 3.551 3.556 3.600 3.644 3.689 3.733 3.778 3.822 3.867 3.911 3.956 4.000	0.269 0.271 0.272 0.274 0.275 0.277 0.278 0.280 0.281 0.283 0.284 0.286 0.287 0.289	0.734 0.746 0.758 0.770 0.782 0.794 0.807 0.819 0.832 0.844 0.857 0.869 0.882 0.895	3.475 4.091 4.740 5.421 6.133 6.873 7.641 8.437 9.258 10.10 10.98 11.87 12.79 13.73 14.69	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
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Return Period	Periods for Predeveloped Flow(cfs)
2 year	0.036097
5 year	0.060553
10 year	0.078894
25 year	0.104157
50 year	0.124334
100 year	0.145571

Return	Periods for Flow(cfs)	Developed	Unmitigated
	0.358405		
	0.91654		
	Return	Flow(cfs) 0.358405 0.48822 0.581688 0.708592 0.809687	0.358405 0.48822 0.581688 0.708592 0.809687

Return	Periods for	Developed	Mitigated
	Flow(cfs)	-	3
	0.02198		
	0.033886		
	0.043924		
	0.059457		
	0.073374		
	0.089549		
	Return	Flow(cfs) 0.02198 0.033886 0.043924 0.059457 0.073374	0.02198 0.033886 0.043924 0.059457 0.073374

Yearly	Peaks for Predevelop	ed and Developed-Mitigated
Year	Predeveloped	Developed
1949	0.050	0.020
1950	0.042	0.020
1951	0.087	0.062
1952	0.021	0.013
1953	0.026	0.039
1954	0.031	0.017
1955	0.029	0-013
1956	0.056	0.045
1957	0.022	0.016
1958	0.023	0.015
1959	0.031	0.020
1960	0.155	0.038
1961	0.046	0.061
1962	0.014	0.014
1963	0.105	0.023
1964	0.041	0.023
1965	0.039	0.019
1966	0.099	0.019
1967	0.048	
1968		0.017
1908	0.024	0.016

1969 1970 1971 1972 1973 1974 1975 1976 1977 1978 1979 1980 1981 1982 1983 1984 1985 1986 1987 1988 1988 1989 1990 1991 1992 1993 1994 1995	0.030 0.021 0.033 0.057 0.021 0.070 0.040 0.043 0.006 0.083 0.045 0.059 0.032 0.049 0.025 0.012 0.018 0.039 0.092 0.027 0.023 0.049 0.027 0.023 0.049 0.044	0.018 0.027 0.022 0.049 0.027 0.018 0.022 0.023 0.016 0.050 0.027 0.045 0.016 0.017 0.020 0.017 0.100 0.019 0.019 0.019 0.019 0.018 0.016 0.015 0.018
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Ranked	Yearly Peaks for	Predeveloped and Developed-Mitigated
WOTIN	bredeverobed.	Developed
1	0.1047	0.0621
2	0.0994	0.0606
3	0.0924	0.0502
4	0.0870	0.0500
5	0.0825	0.0494
6	0.0698	0.0453
7	0.0588	0.0446
8	0.0566	0.0401
9	0.0559	0.0395
10	0.0521	0.0384
11	0.0495	0.0271
12	0.0494	0.0271
13	0.0490	O.O268
14	0.0483	0.0233
15	0.0471	0.0232
16	0.0457	0.0229
17	0.0445	0.0224
18	0.0440	0.0220
19	0.0432	0.0216
20	0.0424	0.0201
21	0.0415	0.0199
22	0.0402	0.0197
23	0.0392	0.0197
24	0.0390	0.0194
25	0.0333	0.0187
26	0.0316	0.0187
27	0.0312	0.0180
28	0.0312	0.0178
29	0.0302	0.0178
30	0.0286	0.0178
31	0.0275	0.0176
32	0.0265	0.0173
33	0.0261	0.0171
34	0.0250	0.0170
35	0.0243	0.0170
36	0.0235	0.0168
37	0.0233	0.0168
38	0.0218	0.0165
39	0.0212	0.0161
40	0.0212	0.0159
		0.0103

41 42 43 44 45 46 47	0.0210 0.0185 0.0159 0.0135 0.0126 0.0119 0.0062	0.0157 0.0156 0.0149 0.0146 0.0145 0.0132
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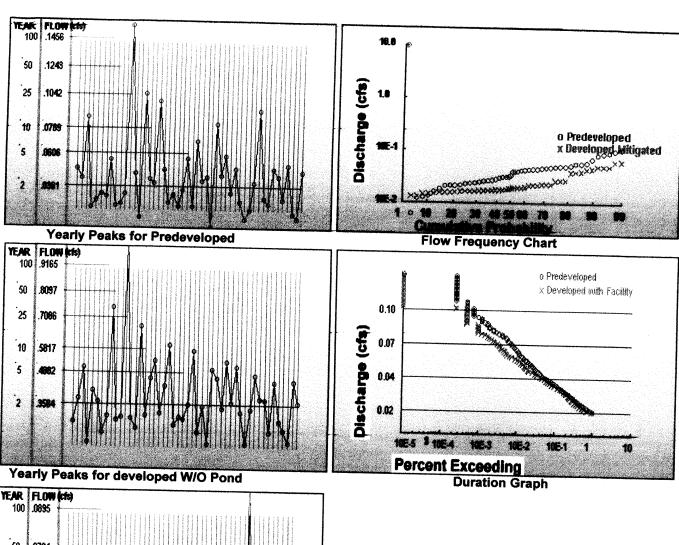
Pilow (CFS) Predev Final Percentage Pass/Fail	1/2 2 ye	ar to 50	year		
0.0180	Flow (CFS	3) Predev	Final	Percentage	Pass/Fail
0.0202 3166 2556 80.0 Pass 0.0213 2780 2258 81.0 Pass 0.0223 2463 1959 79.0 Pass 0.0245 1991 1573 79.0 Pass 0.0256 1805 1437 79.0 Pass 0.0266 1620 1307 80.0 Pass 0.0277 1456 1200 82.0 Pass 0.0288 1310 1105 84.0 Pass 0.0320 937 889 94.0 Pass 0.0320 937 889 94.0 Pass 0.0331 842 814 96.0 Pass 0.0352 667 665 99.0 Pass 0.0353 603 601 99.0 Pass 0.0354 480 414 86.0 Pass 0.0353 482 311 82.0 Pass 0.0363 603 601 P9.0 </td <td></td> <td></td> <td></td> <td></td> <td></td>					
0.0202					Pass
0.0223					
0.0234					Pass
0.0245					Pass
0.0256					Pass
0.0266 1620 1307 80.0 Pass 0.0277 1456 1200 82.0 Pass 0.0299 1174 1015 86.0 Pass 0.0299 1174 1015 86.0 Pass 0.0309 1054 953 90.0 Pass 0.0320 937 889 94.0 Pass 0.0331 842 814 96.0 Pass 0.0342 746 743 99.0 Pass 0.0352 667 665 99.0 Pass 0.0352 667 665 99.0 Pass 0.0363 603 601 99.0 Pass 0.0374 542 514 94.0 Pass 0.0384 480 414 86.0 Pass 0.0395 432 347 80.0 Pass 0.0406 378 311 82.0 Pass 0.0417 332 281 84.0 Pass 0.0427 293 255 87.0 Pass 0.0427 293 255 87.0 Pass 0.0449 236 195 82.0 Pass 0.0449 236 195 82.0 Pass 0.0440 209 173 82.0 Pass 0.0440 184 143 77.0 Pass 0.0492 157 108 68.0 Pass 0.0513 129 83 64.0 Pass 0.0524 120 77 64.0 Pass 0.0556 95 62 65.0 Pass 0.0556 95 62 65.0 Pass 0.0556 95 62 65.0 Pass 0.0558 72 44 61.0 Pass 0.0559 65 38 58.0 Pass 0.0559 65 38 58.0 Pass 0.0559 65 38 58.0 Pass 0.0567 89 54 60.0 Pass 0.0588 72 44 61.0 Pass 0.0599 65 38 58.0 Pass 0.0664 42 19 45.0 Pass 0.0674 39 17 43.0 Pass 0.0664 42 19 45.0 Pass 0.0707 31 14 45.0 Pass					Pass
0.0277 1456 1200 82.0 Pass 0.0288 1310 1105 84.0 Pass 0.0299 1174 1015 86.0 Pass 0.0309 1054 953 90.0 Pass 0.0320 937 889 94.0 Pass 0.0331 842 814 96.0 Pass 0.0342 746 743 99.0 Pass 0.0352 667 665 99.0 Pass 0.0363 603 601 99.0 Pass 0.0374 542 514 94.0 Pass 0.0374 542 514 94.0 Pass 0.0395 432 347 80.0 Pass 0.0406 378 311 82.0 Pass 0.0417 332 281 84.0 Pass 0.0417 332 281 84.0 Pass 0.0447 293 255 87.0 Pass 0.0449 236 195 82.0 Pass 0.0440 209 173 82.0 Pass 0.0470 184 143 77.0 Pass 0.0470 209 173 82.0 Pass 0.0470 184 143 77.0 Pass 0.0470 184 143 77.0 Pass 0.0470 184 143 77.0 Pass 0.0492 157 108 68.0 Pass 0.0503 143 88 61.0 Pass 0.0503 143 88 61.0 Pass 0.0513 129 83 64.0 Pass 0.0554 120 77 64.0 Pass 0.0554 120 77 64.0 Pass 0.05578 89 54 60.0 Pass 0.05578 89 54 60.0 Pass 0.0578 89 54 60.0 Pass 0.0564 42 19 45.0 Pass 0.0664 42 19 45.0 Pass 0.0663 36 16 44.0 Pass 0.0664 42 19 45.0 Pass 0.0665 36 16 44.0 Pass 0.0666 34 15 44.0 Pass 0.0707 31 14 45.0 Pass 0.07079 24 10 41.0 Pass 0.07079 24 10 41.0 Pass 0.07079 24 10 41.0 Pass 0.07092 14 53.0 Pass					Pass
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0.0352 667 665 99.0 Pass 0.0363 603 601 99.0 Pass 0.0374 542 514 94.0 Pass 0.0384 480 414 86.0 Pass 0.0395 432 347 80.0 Pass 0.0406 378 311 82.0 Pass 0.0417 332 281 84.0 Pass 0.0427 293 255 87.0 Pass 0.0438 261 230 88.0 Pass 0.0449 236 195 82.0 Pass 0.0440 209 173 82.0 Pass 0.0470 184 143 77.0 Pass 0.0470 184 143 77.0 Pass 0.0492 157 108 68.0 Pass 0.0513 129 83 64.0 Pass 0.0513 129 83 64.0 Pass 0.0554 120 77 64.0 Pass 0.0554 120 77 64.0 Pass 0.0556 95 62 65.0 Pass 0.0556 95 62 65.0 Pass 0.0578 80 50 62.0 Pass 0.0599 65 38 58.0 Pass 0.0599 65 38 58.0 Pass 0.0610 60 31 51.0 Pass 0.0621 56 27 48.0 Pass 0.0621 56 27 48.0 Pass 0.0663 46 20 43.0 Pass 0.0664 42 19 45.0 Pass 0.0665 36 16 44.0 Pass 0.0677 29 13 44.0 Pass 0.0666 34 15 44.0 Pass 0.0677 29 13 44.0 Pass 0.0669 34 15 44.0 Pass 0.0777 29 13 44.0 Pass 0.0779 24 10 41.0 Pass 0.0779 24 10 41.0 Pass 0.0779 24 10 41.0 Pass 0.0779 14 5 35.0 Pass 0.0779 17 18 7 38.0 Pass 0.0779 18 7 43.0 Pass 0.0779 24 10 41.0 Pass 0.0779 27 47 47 47 47 47 47 47 47 47 47 47 47 47					
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0.0384	0.0374				
0.0395	0.0384	480			
0.0406 378 311 82.0 Pass 0.0417 332 281 84.0 Pass 0.0427 293 255 87.0 Pass 0.0438 261 230 88.0 Pass 0.0449 236 195 82.0 Pass 0.0460 209 173 82.0 Pass 0.0470 184 143 77.0 Pass 0.0481 171 126 73.0 Pass 0.0492 157 108 68.0 Pass 0.0503 143 88 61.0 Pass 0.0503 143 88 61.0 Pass 0.0513 129 83 64.0 Pass 0.0524 120 77 64.0 Pass 0.0546 105 67 63.0 Pass 0.0556 95 62 65.0 Pass 0.0578 80 50 62.0 Pass 0.0599 65 38 58.0 Pass 0.0	0.0395	432	347		
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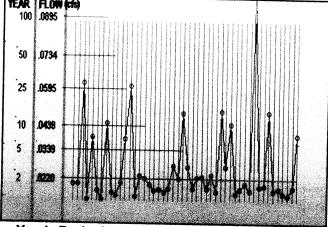
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On-line facility volume: 0.138 acre-feet On-line facility target flow: 0.15 cfs.

Adjusted for 15 min: 0.17 cfs.

Off-line facility target flow: 0.09 cfs. Adjusted for 15 min: 0.1 cfs.





Yearly Peaks for Developed W/Pond

Project Name: LID Road Section

Site Address:

City

Report Date : 7/27/2004 Gage : McMillian

Data Start : 1948 Data End : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

Basin : Pre-Dev
Flows To : Point of Compliance

GroundWater: No

Land Use

Acres

TILL FOREST: 1.64

DEVELOPED LAND USE

Basin : Dev

Flows To : BR Swale

GroundWater: No

Land Use

Acres

TILL GRASS:

0.41

IMPERVIOUS:

1.23

RCHRES (POND) INFORMATION Pond Name:

Pond Name: BR Swale
Pond Type: Trapezoidal Pond

Pond Flows to : Pond 2

Pond Rain / Evap is not activated. Dimensions

Depth: 1ft. Bottom Length: 720ft. Bottom Width: 4ft. Side slope 1: 3 To 1 Side slope 2: 3 To 1 Side slope 3: 3 To 1 Side slope 4: 3 To 1

Volume at Riser Head: 0.046 acre-ft. 96.8% of runoff infilrated through small

Discharge Structure Riser Height: 0.5 ft.

Riser Diameter: 12 in.

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt(cfs)
0.000	0.066	0.000	0.000	0.000
0.100	0.076	0.007	0.000	0.067
0.200	0.086	0.015	0.000	0.067
0.300	0.096	0.024	0.000	0.067
0.400	0.106	0.034	0.000	0.067
0.500	0.116	0.046	0.000	0.067
0.600	0.126	0.058	0.308	0.067
0.700	0.136	0.071	0.871	0.067

0_800	0-146	0.085	1.600	0.067
0.900	0.157	0.100	2.464	0.067
1.000	0.167	0.116	3.443	0.067

Pond Name: Pond 2

Pond Type: Trapezoidal Pond
Pond Flows to : Point of Compliance
Pond Rain / Evap is not activated.

Dimensions

Depth: 4ft.

Bottom Length: 80.92ft.

Bottom Width: 26.98ft.

Side slope 1: 3 To 1

Side slope 2: 3 To 1

Side slope 3: 3 To 1

Side slope 4: 3 To 1

Volume at Riser Head: 0.225 acre-ft. 9601 CF -> 363 W Discharge Structure

Riser Height: 3 ft.
Riser Diameter: 18 in.
NotchType : Rectangular
Notch Width : 0.010 ft.
Notch Height: 1.032 ft.

Orifice 1 Diameter: 0.729 in. Elevation: 0 ft.

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt(cfs)
0.000	0.050	0.000	0.000	0.000
0.044	0.051	0.002	0.003	0.000
0.089	0.051	0.005	0.004	0.000
0.133	0.052	0.007	0.005	0.000
0.178	0.053	0.009	0.006	0.000
0.222	0.053	0.012	0.007	0.000
0.267	0.054	0.014	0.007	0.000
0.311	0.055	0.016	0.008	0.000
0.356	0.056	0.019	0.008	σ.000
0.400	0.056	0.021	0.009	0.000
0.444	0.057	0.024	0.009	0.000
0.489	0.058	0.026	0.010	0.000
0.533	0.058	0.029	0.010	0.000
0.578	0.059	0.031	0.011	0.000
0.622	0.060	0.034	0.011	0.000
0.667	0.060	0.037	0.011	0.000
0.711	0.061	0.039	0.012	0.000
0.756	0.062	0.042	0.012	0.000
0.800	0.063	0.045	0.012	0.000
0.844	0.063	0.048	0.013	0.000
0.889	0.064	0.051	0.013	0.000
0.933	0.065	0.053	0.013	0.000
0.978	0.065	0.056	0.014	0.000
1.022	0.066	0.059	0.014	0.000
1.067	0.067	0.062	0.014	0.000
1.111	0.068	0.065	0.015	0.000
1.156	0.068	0.068	0.015	0.000
1.200	0.069	0.071	0.015	0.000
1.244	0.070	0.074	0.016	0.000
1.289	0.071	0.078	0.016	0.000
1.333	0.071	0.081	0.016	0.000
1.378	0.072	0.084	0.016	0.000
1.422	0.073	0.087	0.017	0.000
1.467	0.074	0.090	0.017	0.000
1.511	0.074	0.094	0.017	0.000
1.556	0.075	0.097	0.017	0.000
1.600	0.076	0.100	0.018	0.000
1.644	0.077	0.104	0.018	0-000
1.689	0.078	0.107	0.018	0.000
1.733	0.078	0.111	0.018	0.000
1.778	0.079	0.114	0.019	0.000
1.822	0.080	0.118	0.019	0-000
1.867	0.081	0.121	0.019	0.000

1.911 1.956 2.000	0.082 0.082 0.083	0.125 0.128 0.132	0.019 0.020 0.020	0.000
2.044	0.084	0.136	0.020	0.000
2.089 2.133	0.085 0.086	0.140	0.022	0.000
2.178	0.086	0.143 0.147	0.023 0.024	0.000 0.000
2.222	0.087	0.151	0-025	0.000
2.267 2.311	0.088	0.155	0.026	0.000
2.356	0.089 0.090	0.159 0.163	0.027 0.029	0.000
2.400	0.091	0.167	0.030	0.000 0.000
2.444	0.091	0.171	0.032	0.000
2.489 2.533	0.092 0.093	0.175 0.179	0.033	0.000
2.578	0.094	0.179	0.035 0.036	0.000 0.000
2.622	0.095	0.187	0.038	0.000
2.667 2.711	0.096	0.192	0.040	0.000
2.756	0.096 0.097	0.196 0.200	0.041 0.043	0.000
2.800	0.098	0.205	0.043	0.000 0.000
2.844	0.099	0.209	0.046	0.000
2.889 2.933	0.100	0.213 0.218	0.048	0.000
2.978	0.102	0.222	0.049 0.051	0.000
3.022	0.103	0.227	0.101	0.000
3.067 3.111	0.103 0.104	0.232 0.236	0.304	0.000
3.156	0.105	0.236	0.594 0.949	0.000 0.000
3.200	0.106	0.246	1.360	0.000
3.244 3.289	0.107 0.108	0.250	1.819	0.000
3.333	0.108	0.255 0.260	2.322 2.865	0.000 0.000
3.378	0.110	0.265	3.446	0.000
3.422 3.467	0.111 0.112	0.270	4.062	0.000
3.511	0.112	0.275 0.280	4.711 5.392	0.000
3.556	0.113	0.285	6.103	0.000
3.600 3.644	0.114	0.290	6.844	0.000
3.689	0.115 0.116	0.295 0.300	7.612 8.407	0.000
3.733	0.117	0.305	9.229	0.000 0.000
3.778	0.118	0.310	10.08	0.000
3.822 3.867	0.119 0.120	0.316 0.321	10.95 11.84	0.000
3.911	0.121	0.321	12.76	0.000 0.000
3.956	0.122	0.332	13.70	0.000
4.000	0.123	0.337	14.66	0.000

Flow Frequency Return	Periods for Predeveloped
Return Period	Flow(cfs)
2 year	0.036097
5 year	0.060553
10 year	0.078894
25 year	0.104157
50 year	0.124334
100 year	0.145571

Flow Frequency Return	Periods for Developed Unmitigated
Return Period	Flow(cfs)
2 year	0.376885
5 year	0.511138
10 year	0.607475
25 year	0.737928
50 year	0.841609
100 year	0.950993

Flow Frequency Return Period	Return Periods for Developed Mitigated
10 year	
25 year	0.180161
50 year	0.324577
IOO year	0.566883
2 year 5 year 10 year 25 year	0.324577

Yearly	Peaks for Prede	eveloped and Developed-Mitigated
Year	Predevelo	oped Developed Filtigated
1949	0.050	0.012
1950	0.042	0.012
1951	0.087	0.012
1952	0.021	
1953	0.026	0.000
1954	0.031	0.007
1955	0.029	0.010
1956	0.056	0.010
1957	0.022	0.015
1958	0.023	0.012
1959	0.023	0.007
1960	0.155	0.009
1961		0.026
1962	0.046	0.011
1963	0.014	0.005
1964	0.105	0.017
1965	0.041	0.012
	0.039	0.012
1966	0.099	0.004
1967	0.048	0.013
1968	0.024	0.011
1969	0.030	0.011
1970	0.021	0.011
1971	0.033	0.011
1972	0.057	0.014
1973	0.021	σ.010
1974	0.070	Q.008
1975	0.040	0.012
1976	0.043	0.007
1977	0.006	0.009
1978	0.083	0.016
1979	0.045	0.013
1980	0.059	0.018
1981	0.032	0.011
1982	0.049	0.013
1983	0.025	0.018
1984	0.012	0.018
1985	0.018	0.009
1986	0.039	0.015
1987	0.092	0.151
1988	0.027	0.131
1989	0.023	0.008
1990	0.049	
1991	0.044	0.015
1992	0.027	0.018
1993	0.052	0.013
1994		0.016
1995	0.016	0.000
1996	0.013	0.017
1990	0.047	0.013

Ranked Rank	Yearly Peaks for Predeveloped	Predeveloped and Developed-Mitigated
1		Developed
<u>.</u>	0.1047	0.0259
2	0.0994	0.0239
3	0.0924	0.0182
4	0.0870	0.0181
5	0.0825	0.0181
6	0.0698	0.0176
7	0.0588	0.0170
Ω	0 0566	0 0160

9-10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 33 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47	0.0559 0.0521 0.0495 0.0494 0.0490 0.0483 0.0471 0.0457 0.0445 0.0440 0.0432 0.0424 0.0415 0.0402 0.0392 0.0390 0.0333 0.0316 0.0312 0.0313 0.0215 0.0250 0.0265 0.0261 0.0250 0.0265 0.0261 0.0250 0.0212 0.0212 0.0212 0.0212 0.0212 0.0212 0.0212 0.0212 0.0119 0.0062	0.0159 0.0157 0.0154 0.0150 0.0146 0.0145 0.0132 0.0132 0.0131 0.0130 0.0128 0.0125 0.0120 0.0120 0.0119 0.0119 0.0119 0.0111 0.0111 0.0111 0.0110 0.0107 0.0104 0.0102 0.0098 0.0093 0.0093 0.0093 0.0093 0.0095 0.0075 0.0075 0.0075 0.0075 0.0070 0.0052 0.0042 0.0000
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1/2 2 yea	r to 50	year		
Flow(CFS)	Predev	Final	Percentage	Pass/Fail
0.0180	4176	195	4.0	Pass
0.0191	3628	125	3.0	Pass
0.0202	3166	83	2.0	Pass
0.0213	2780	71	2.0	Pass
0.0223	2463	59	2.0	Pass
0.0234	2202	45	2.0	Pass
0.0245	1991	36	1.0	Pass
0.0256	1805	33	1.0	Pass
0.0266	1620	28	1.0	Pass
0.0277	1456	27	1.0	Pass
0.0288	1310	25	1.0	Pass
0.0299	1174	24	2.0	Pass
0.0309	1054	22	2.0	Pass
0.0320	937	21	2.0	Pass
0.0331	842	20	2.0	Pass
0.0342	746	19	2.0	Pass
0.0352	667	17	2.0	Pass
0.0363	603	16	2.0	Pass
0.0374	542	15	2.0	Pass
0.0384	480	14	2.0	Pass
0.0395	432	12	2.0	Pass
0.0406	378	11	2.0	Pass
0.0417	332	10	3.0	Pass
0.0427	293	10	3.0	Pass
0.0438	261	9	3.0	Pass
0.0449	236	7	2.0	Pass
0.0460	209	6	2.0	Pass
0.0470	184	6	3.0	Pass
0.0481	171	5	2.0	Pass

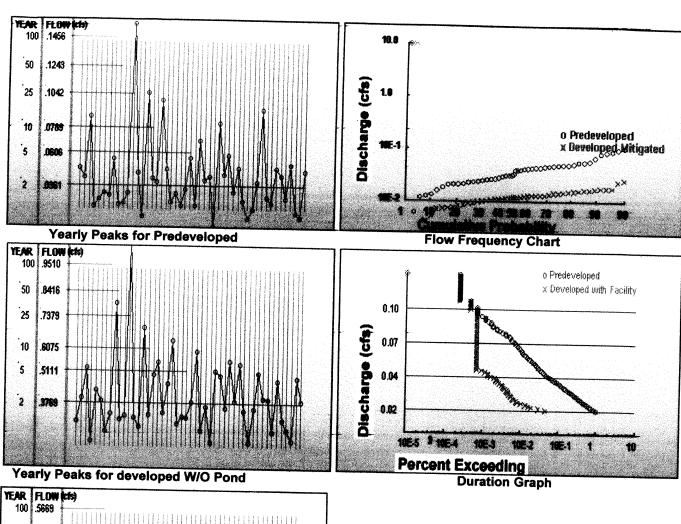
0.0492	157	4	2.0	D
0.0503	143	4: 3	2.0	Pass Pass
0.0513	129	3	2.0	Pass
0.0524	120	3	2.0	Pass
0.0535	114	3	2.0	Pass
0.0546	105	3	2.0	Pass
0.0556 0.0567	95 89	3 3	3.0 3.0	Pass
0.0578	80		3.0	Pass Pass
0.0588	72	3 3	4.0	Pass
0.0599	65	3	4.0	Pass
0.0610	60	3 3 3 3	5.0	Pass
0.0621 0.0631	56 50	3	5.0 6.0	Pass
0.0642	47	3	6.0	Pass Pass
0.0653	46	3.	6.0	Pass
0.0664	42	3	7.0	Pass
0.0674	39	3	7.0	Pass
0.0685 0.0696	36 34	3 3	8.0 8.0	Pass Pass
0.0707	31	3	9.0	Pass
0.0717	29	3	10.0	Pass
0.0728	26	3	11.0	Pass
0.0739 0.0749	2 4 23	3 3	12.0 13.0	Pass
0.0760	22	3	13.0	Pass Pass
0.0771	18	3	16.0	Pass
0.0782	17	3	17.0	Pass
0.0792 0.0803	14 12	3	21.0 25.0	Pass
0.0814	10	3	30.0	Pass Pass
0.0825	10	3	30.0	Pass
0.0835	8	3	37.0	Pass
0.0846 0.0857	8 7	3	37.0	Pass
0.0868	7	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	42.0 42.0	Pass Pass
0.0878	6	3	50.0	Pass
0.0889	5	3	60.0	Pass
0.0900	5 5	3	60.0	Pass
0.0911 0.0921	5 4	3	60.0 75.0	Pass Pass
0.0932	3		100.0	Pass
0.0943	3	3 3 3	100.0	Pass
0.0953	3	3	100.0	Pass
0.0964 0.0975	3 3	3	100.0	Pass
0.0986	3	2	66.0	Pass Pass
0.0996	2	2	100.0	Pass
0.1007	3 3 2 2 2	2	100.0	Pass
0.1018 0.1029	2	2 2 2 2 2 2	100.0 100.0	Pass Pass
0.1039	2	1	50.0	Pass
0.1050	1	1	100.0	Pass
0.1061	1	1	100.0	Pass
0.1072 0.1082	1 1	1 1	100.0 100.0	Pass
0.1093	1	1	100.0	Pass Pass
0.1104	1	1	100.0	Pass
0.1115	1	1	100.0	Pass
0.1125 0.1136	1	1	100.0	Pass
0.1136	1	1	100.0 100.0	Pass Pass
0.1157	1	1	100.0	Pass
0.1168	1	1	100.0	Pass
0.1179 0.1190	1 1	1 1	100.0 100.0	Pass
0-1200	1.	1	100.0	Pass Pass
0.1211	1	1	100.0	Pass
0.1222	1	1	100.0	Pass
0.1233 0.1243	1 1	1 1	100.0 100.0	Pass Pass
J • 16 4 J	-	1	100.0	газз

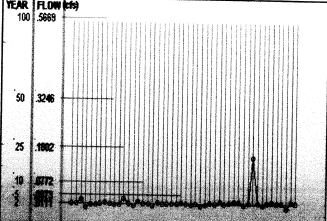
On-line facility volume: 0.138 acre-feet On-line facility target flow: 0.15 ofs.

Adjusted for 15 min: 0.17 cfs.

Off-line facility target flow: 0.09 cfs.

Adjusted for 15 min: 0.1 cfs.





Yearly Peaks for Developed W/Pond

APPENDIX C

WWHM Output for Impervious Pavement vs. Pervious Pavement Modeled as Grass

Project Name: impervious

Site Address:

City

Report Date : 7/28/2004
Gage : McMillian

Data Start: 1948
Data End: 1996
Precip Scale: 1.00

PREDEVELOPED LAND USE

Basin : Basin 1

Flows To : Point of Compliance

GroundWater: No

Land Use

TILL FOREST:

ACTOS

DEVELOPED LAND USE

Basin : Basin 1 Flows To : Pond 1

GroundWater: No

Land Use

Acres

IMPERVIOUS: 0.5

RCHRES (POND) INFORMATION Pond Name: Pond 1

Pond Type: Trapezoidal Pond
Pond Flows to: Point of Compliance
Pond Rain / Evep is not activated.

Dimensions

Depth: 5ft.
Bottom Length: 69.39ft.
Bottom Width: 23.12ft.
Side slope 1: 3 To 1
Side slope 2: 3 To 1
Side slope 3: 3 To 1
Side slope 4: 3 To 1

Volume at Riser Head: 0.267 acre-ft. 11630 cF /21780 = 0.534 cF/SF → 0.02 cg/SF

Discharge Structure
Riser Height: 4 ft.
Riser Diameter: 18 in.
NotchType : Rectangular
Notch Width : 0.010 ft.
Notch Height: 0.876 ft.

Orifice 1 Diameter: 0.337 in. Elevation: 0 ft.

Stage (It)	WIAG (SCL)	VOLUMe (acr-ft)	Dschrg(cfs)	Infilt(cfs)
0.000 0.056 0.111 0.167	0.037 0.038 0.038 0.039	0.000 0.002 0.004 0.006	0.000 0.001 0.001 0.001	0.000 0.000 0.000 0.000 0.000
0.222	0.040	0.009	0.001	0.000

	002 0.000 002 0.000 002 0.000 002 0.000 002 0.000 002 0.000 003 0.000 003 0.000 003 0.000 003 0.000 003 0.000 003 0.000 003 0.000 003 0.000 003 0.000 003 0.000 003 0.000 003 0.000 003 0.000 003 0.000 003 0.000 004 0.000 04 0.000 04 0.000 04 0.000 04 0.000 04 0.000 05 0.000 05 0.000 05 0.000 05 0.000 05 0.000 05 <
0.002 0.002 0.002 0.002 0.002	0.002 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005
0.011	0.015 0.018 0.020 0.022 0.025 0.027 0.030 0.033 0.035 0.038 0.041 0.043 0.046 0.049 0.052 0.055 0.058 0.061 0.064 0.067 0.071 0.074 0.077 0.080 0.084 0.087 0.091 0.094 0.098 0.101 0.105 0.109 0.113 0.116 0.120 0.124 0.128 0.132 0.136 0.140 0.145 0.149 0.153 0.157 0.162 0.166 0.171 0.175 0.180
0.040	0.042 0.043 0.043 0.044 0.045 0.046 0.047 0.048 0.050 0.050 0.051 0.052 0.053 0.054 0.055 0.055 0.055 0.056 0.057 0.058 0.066 0.066 0.066 0.066 0.067 0.068 0.067 0.068 0.070 0.072 0.073 0.075 0.088 0.
0.278 0.333 0.389	0.444 0.500 0.6556 0.611 0.667 0.722 0.778 0.889 0.944 1.000 1.056 1.111 1.167 1.222 1.278 1.333 1.389 1.444 1.500 1.556 1.611 1.667 1.722 1.778 1.833 1.889 1.944 2.000 2.056 2.111 2.167 2.222 2.278 2.333 2.389 2.444 2.500 2.556 2.611 2.667 2.722 2.778 2.833 2.889 2.944 3.000

4.278 4.333 4.389 4.444 4.500 4.556 4.611 4.667 4.722 4.778 4.833 4.889 4.944 5.000	0.106 0.108 0.109 0.110 0.111 0.112 0.113 0.114 0.115 0.117 0.118 0.119 0.120	0.296 0.302 0.308 0.314 0.320 0.326 0.332 0.339 0.345 0.351 0.358 0.365 0.371	2.167 2.840 3.572 4.357 5.194 6.078 7.008 7.981 8.995 10.05 11.14 12.27 13.44	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
5.000	0.120	0.371 0.378	13.44 14.64	0.000 0.000

Flow Frequency Retur	n Periods for Predeveloped
Return Period	Flow(cfs)
2 year	0.011005
5 year	0.018461
10 year	0.024053
25 year	0.031755
50 year	0.037907
100 year	0.044381

Flow Frequency Re	turn Periods for Developed Unmitigated
Return Period	Flow(cfs)
2 year	0.143725
5 year	0.191858
10 year	0,22598
25 year	0.271745
50 year	0.307814
100 year	0.345618

	u
Flow(cfs)	
0.006053	
0.010037	
0.013592	
0.019362	
0.024756	
0.031245	
	0.006053 0.010037 0.013592 0.019362 0.024756

Year	Predeveloped	ed and Developed-Mitigat
1949	0.015	Developed
1950		0.005
1951	0.013	0.005
	0.027	0.023
1952	0.006	0.004
1953	0.008	0.014
1954	0.010	0.005
1955	0.009	0.004
1956	0.017	0.020
1957	0.007	0.005
1958	0.007	0.004
1959	0.010	0.005
1960	0.047	0.008
1961	0.014	0.024
1962	0.004	0.004
1963	0.032	0.005
1964	0-013	0.005
1965	0.012	0.005
1966	0.030	0.005
1967	0.015	
1968		0.005
	0.007	0.004
1969	0.009	0.005

1970 1971 1972 1973 1974	0.006 0.010 0.017 0.006 0.021	0.006 0.005 0.019 0.005 0.005
1975	0.012	0.005
1976	0.013	0.005
1977	0.002	0.005
1978	0.025	Q.005
1979	0.014	0.004
1980	0.018	0.015
1981	0.010	0,005
1982	0.015	0.015
1983	0.008	0.005
1984	0.004	0.005
1985	0.006	0.005
1986	0.012	0,005
1987	0.028	0.028
1988	0.008	0.005
1989 1990	0.007	0.005
1990	0.015	0.016
1992	0.013	0.005
1993	0.008 0.016	0.005
1994	0.005	0.004
1995	0.003	0.004 0.005
1996	0.014	0.003

Ranked	rearry Peaks for	Predeveloped and Developed-Mitigated
Rank	Predeveloped	Developed
	_	

Rank	Predeveloped	Develope
1	0.0319	0.0236
2	0.0303	0.0233
3	0.0282	0.0196
4	0.0265	0.0192
5	0.0252	0.0161
6	0.0213	0_0154
7	0.0179	0.0153
8	0.0172	0.0144
9	0.0170	0.0121
10	0.0159	0.0076
11	0.0151	0.0061
12	0.0151	0.0056
13	0.0149	0.0055
14	0.0147	0.0052
15	0.0144	0.0052
16	0.0139	0.0052
17	0.0136	0.0052
18	0.0134	0.0052
19	0.0132	0.0052
20	0.0129	0.0052
21	0.0126	0.0052
22	0.0122	0.0052
23	0.0119	0.0052
24	0.0119	0.0052
25 26	0.0102	0.0052
27	0.0096	0.0051
28	0.0095	0.0051
29	0.0095 0.0092	0_0050
30	0.0092	0.0050
31	0.0084	0.0050
32	0.0081	0.0049
33	0.0080	0.0048
34	0.0076	0.0048 0.0047
35	0.0074	0.0047
36	0.0072	0.0047
37	0.0071	0.0046
38	0.0066	0.0046
39	0.0065	0.0045
40	0.0065	0.0045
41	0.0064	0.0043
*		0.0044

42.	0.0056	0.0044
43	0.0048	0.0044
44	0.0041	0.0041
45	0.0038	0.0041
46	0.0036	0.0040
47	0.0019	0.0037

1/2 2 Year 10 50 Year Flow (CFS) Prodev Final Percentage Pass / Fail 0.0055 3628 1759 48.0 Pass 0.0062 3164 1606 50.0 Pass 0.0065 2776 1493 53.0 Pass 0.0068 2463 1350 54.0 Pass 0.0075 1991 1161 58.0 Pass 0.0075 1991 1161 58.0 Pass 0.0078 1805 1082 59.0 Pass 0.0078 1456 968 66.0 Pass 0.0084 1456 968 66.0 Pass 0.0084 1456 968 66.0 Pass 0.0098 1310 905 69.0 Pass 0.0094 1054 790 74.0 Pass 0.0094 1054 790 74.0 Pass 0.0094 1054 790 74.0 Pass 0.0101 843 675 80.0 Pass 0.0101 843 675 80.0 Pass 0.0111 603 514 85.0 Pass 0.0111 603 514 85.0 Pass 0.0111 603 514 85.0 Pass 0.0117 480 436 90.0 Pass 0.0117 480 436 90.0 Pass 0.0120 434 399 91.0 Pass 0.0120 434 399 91.0 Pass 0.0124 378 370 97.0 Pass 0.0124 378 370 97.0 Pass 0.0124 378 370 97.0 Pass 0.0134 263 272 103.0 Pass 0.0134 263 272 103.0 Pass 0.0147 271 164 95.0 Pass 0.0143 184 187 101.0 Pass 0.0143 184 187 101.0 Pass 0.0143 184 187 101.0 Pass 0.0153 143 131 91.0 Pass 0.0153 143 131 91.0 Pass 0.0153 143 131 91.0 Pass 0.0166 105 94 89.0 Pass 0.0166 105 94 99.0					1
	1/2 2 year to 50 year				
0.0055	Flow (CF			Percentage	Dace (Fail
0.0058 3628 1759 48.0 Pass 0.0062 3164 1606 50.0 Pass 0.0065 2776 1493 53.0 Pass 0.0068 2463 1350 54.0 Pass 0.0071 2201 1251 56.0 Pass 0.0077 1991 1161 58.0 Pass 0.0078 1805 1082 59.0 Pass 0.0078 1805 1082 59.0 Pass 0.0081 1618 1023 63.0 Pass 0.0084 1456 968 66.0 Pass 0.0088 1310 905 69.0 Pass 0.0098 1310 905 69.0 Pass 0.0099 1173 847 72.0 Pass 0.0098 937 723 77.0 Pass 0.0101 843 675 80.0 Pass 0.0111 603 514 85.0 Pass 0.0111 603 514 85.0 Pass 0.0111 603 514 87.0 Pass 0.0114 343 474 87.0 Pass 0.0117 480 436 90.0 Pass 0.0120 434 399 91.0 Pass 0.0124 378 370 97.0 Pass 0.0127 332 335 100.0 Pass 0.0127 332 335 100.0 Pass 0.0130 293 300 102.0 Pass 0.0137 236 242 102.0 Pass 0.0137 236 242 102.0 Pass 0.0143 184 187 101.0 Pass 0.0147 171 164 95.0 Pass 0.0150 158 148 93.0 Pass 0.0150 158 148 93.0 Pass 0.0151 149 89 99.0 Pass 0.0151 149 89.0 Pass 0.0156 129 118 91.0 Pass 0.0156 129 118 91.0 Pass 0.0166 105 94 89.0 Pass 0.0173 89 82 92.0 Pass 0.0166 105 94 89.0 Pass 0.0173 89 82 92.0 Pass 0.0173 89 82 92.0 Pass 0.0174 80 78 97.0 Pass 0.0175 31 299 93.0 Pass 0.0176 80 78 97.0 Pass 0.0177 95.0 Pass 0.0178 95 87 91.0 Pass 0.0186 60 64 106.0 Pass 0.0199 46 44 95.0 Pass 0.0199 46 44 95.0 Pass 0.0199 246 44 95.0 Pass 0.0199 250 53 105.0 Pass 0.0199 26 89.0 Pass 0.0199 27 828 0.0199 39 100.0 Pass 0.0199 46 44 95.0 Pass 0.0199 29 20 Pass 0.0199 29 20 Pass 0.0199 39 100.0 Pass 0.0199 39 100.0 Pass 0.0199 46 44 95.0 Pass 0.0199 46 44 95.0 Pass 0.0199 29 20 Pass 0.0199 39 100.0 Pass 0.0222 26 25 96.0 Pass 0.0222 26 25 96.0 Pass 0.0223 19 92.0 Pass 0.0222 26 25 96.0 Pass 0.0223 19 92.0 Pass 0.0224 14 9 64.0 Pass 0.0225 12 8 66.0 Pass 0.0225 12 9 93.0 Pass					
0.0065		3628			
0.0066	0.0062				
0.0068			1493		
0.0075			1350		
0.0078				56.0	
0.0081 1618 1082 59.0 Pass 0.0084 1456 968 66.0 Pass 0.0088 1310 905 69.0 Pass 0.0091 1173 847 72.0 Pass 0.0098 937 723 77.0 Pass 0.0101 843 675 80.0 Pass 0.0104 746 617 82.0 Pass 0.0107 670 566 84.0 Pass 0.0111 603 514 85.0 Pass 0.0114 543 474 87.0 Pass 0.0114 543 474 87.0 Pass 0.0120 434 399 91.0 Pass 0.0124 378 370 97.0 Pass 0.0127 332 335 100.0 Pass 0.0130 293 300 102.0 Pass 0.0130 293 300 102.0 Pass 0.0140 210 208 99.0 Pass 0.0143 184 187 101.0 Pass 0.0147 171 164 95.0 Pass 0.0150 158 148 93.0 Pass 0.0156 129 118 91.0 Pass 0.0156 129 118 91.0 Pass 0.0166 105 94 89.0 Pass 0.0173 89 82 92.0 Pass 0.0183 65 69 106.0 Pass 0.0199 46 44 95.0 Pass 0.0199 46 97.0 Pass 0.0199 97.0 Pass					
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0.0225 24 20 83.0 Pass 0.0229 23 19 82.0 Pass 0.0232 22 15 68.0 Pass 0.0235 18 12 66.0 Pass 0.0238 17 10 58.0 Pass 0.0242 14 9 64.0 Pass 0.0245 12 8 66.0 Pass 0.0248 10 8 80.0 Pass 0.0255 8 7 70.0 Pass					
0.0229 23 19 82.0 Pass 0.0232 22 15 68.0 Pass 0.0235 18 12 66.0 Pass 0.0238 17 10 58.0 Pass 0.0242 14 9 64.0 Pass 0.0245 12 8 66.0 Pass 0.0248 10 8 80.0 Pass 0.0251 10 7 70.0 Pass					. *
0.0232 22 15 68.0 Pass 0.0235 18 12 66.0 Pass 0.0238 17 10 58.0 Pass 0.0242 14 9 64.0 Pass 0.0245 12 8 66.0 Pass 0.0248 10 8 80.0 Pass 0.0251 10 7 70.0 Pass					
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0.0242 14 9 64.0 Pass 0.0245 12 8 66.0 Pass 0.0248 10 8 80.0 Pass 0.0251 10 7 70.0 Pass					
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	0.0255	8	7	87.0	

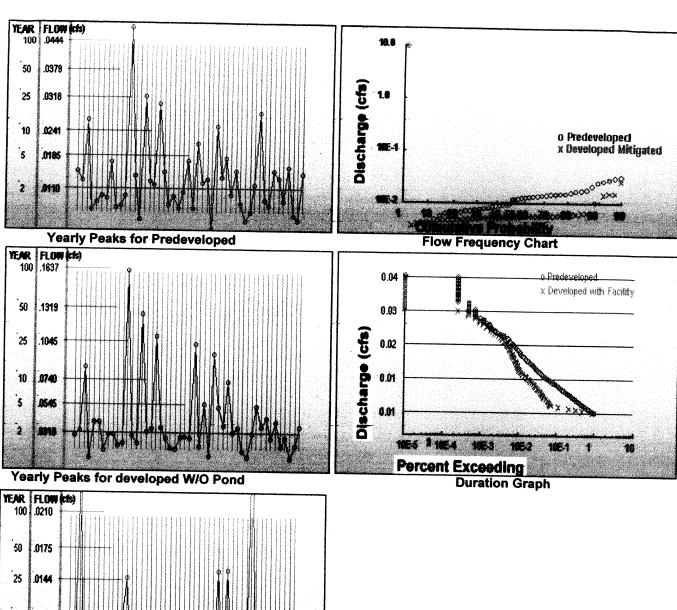
0.0258 0.0261 0.0265 0.0268 0.0271 0.0274 0.0278 0.0281 0.0284 0.0297 0.0291 0.0294 0.0297 0.0301 0.0314 0.0317 0.0320 0.0314 0.0317 0.0320 0.0323 0.0327 0.0330 0.0340 0.0340 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0366 0.0366 0.0369 0.0379	87765543333322221111111111111111111111111111	6655332000000000000000000000000000000000	75.0 85.0 71.0 83.0 60.0 60.0 40.0 .0 .0 .0 .0 .0 .0 .0 .0	Pass ss
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On-line facility volume: 0.054 acre-feet 2352 CF / On-line facility target flow: 0.06 cfs.

2352 CF /21780 = 0.108 CF/SF -> 0.004 CY/SF

On-line facility target flow: 0.06 cfs. Adjusted for 15 min: 0.07 cfs. Off-line facility target flow: 0.03 cfs.

Adjusted for 15 min: 0.04 cfs.



50 .0175 25 .0144 10 .9109 5 .0088

Yearly Peaks for Developed W/Pond

Project Name: perv_grass

Site Address:

City

Report Date : 7/28/2004 Gage : McMillian Data Start : 1948

Data End : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

Basin

: Basin 1

Flows To : Point of Compliance

GroundWater: No

Land Use

Acres

TILL FOREST:

DEVELOPED LAND USE

Basin : Basin 1 Flows To : Pond 1 GroundWater: No

Land Use

Acres

TILL GRASS:

0.5

RCHRES (POND) INFORMATION

Pond Name: Pond 1
Pond Type: Trapezoidal Pond

Pond Flows to : Point of Compliance Pond Rain / Evap is not activated.

Dimensions

Depth: 4ft. Bottom Length: 44.7ft. Bottom Width: 14.89ft. Side slope 1: 3 To 1 Side slope 2: 3 To 1 Side slope 3: 3 To 1

Volume at Riser Head: 0.090 acre-ft. 3920 CF /21780 = 0.18 CF/SF -> 0.007 CM/SF Discharge Structure

Discharge Structure Riser Height: 3 ft. Riser Diameter: 18 in. NotchType : Rectangular Notch Width: 0.000 ft. Notch Height: 0.000 ft.

Orifice 1 Diameter: 0.39 in. Elevation: 0 ft.

SCAGE (IC)	Area (acr)	AOTOMO (SCL-LT)	Dschrg(cfs)	Infilt (cfs)
0.000	0.015	0,000	0.000	0.000
0.044	0.016	0.001	0.001	0.000
0.089	0.016	0.001	0.001	0.000
0.133	0.016	0.002	0.001	0.000
0.178	0.017	0.003	0.002	0.000

0-222 0-017 0-004 0-002 0.000	
0-222	
0.311 0.018 0.005 0.002 0.000	
0.356 0.018 0.006 0.002 0.000	
0.400 0.019 0.007 0.003 0.000	
0.444 0.019 0.008 0.003 0.000	
0.489	
0.578 0.020 0.010 0.003 Q.000	
0.622 0.021 0.011 0.003 0.000	
0.667 0.021 0.012 0.003 0.000	
0.711 0.022 0.013 0.003 0.000	
0.756 0.022 0.014 0.003 0.000	
0.800 0.022 0.015 0.004 0.000 0.844 0.023 0.016 0.004 0.000	
0.889 0.023 0.017 0.004 0.000	
0.933 0.024 0.018 0.004 0.000	
0.978 0.024 0.019 0.004 0.000	
$egin{array}{cccccccccccccccccccccccccccccccccccc$	
$egin{array}{cccccccccccccccccccccccccccccccccccc$	
1.156 0.026 0.024 0.004 0.000	
1-200 0-026 0-025 0-004 0-000	
1.244 0.027 0.026 0.004 0.000	
1.289 0.027 0.027 0.005 0.000 1.333 0.028 0.028 0.005 0.000	
1.333	
1.422 0.029 0.031 0.005 0.000	
1.467 0.029 0.032 0.005 0.000	
1.511 0.030 0.033 0.005 0.000 1.556 0.030 0.035 0.005 0.000	
1.556 0.030 0.035 0.005 0.000 1.600 0.031 0.036 0.005 0.000	
1.644 0.031 0.037 0.005 0.000	
1.689 0.031 0.039 0.005 0.000	
1.733 0.032 0.040 0.005 0.000	
1.778	
1.822	
1.911 0.034 0.046 0.006 0.000	
1.956 0.034 0.048 0.006 0.000	
2.000 0.035 0.049 0.006 0.000	
2.044	
2.133 0.037 0.054 0.006 0.000	
2_178	
2.222 0.038 0.057 0.006 0.000	
2.267	
2.311 0.039 0.061 0.006 0.000 2.356 0.039 0.062 0.006 0.000	
2.400 0.040 0.064 0.006 0.000	
2.444 0.040 0.066 0.006 0.000	
2.489	
2.533	
2.622 0.042 0.073 0.006 0.000	
2.667 0.043 0.075 0.007 0.000	
2.711 0.044 0.077 0.007 0.000	
2.756	
2.844 0.045 0.083 0.007 0.000	
2.889 0.046 0.085 0.007 0.000	
2.933 0.046 0.087 0.007 0.000	
2.978	
3.022 0.048 0.091 0.055 0.000 3.067 0.048 0.093 0.258 0.000	
3.111 0.049 0.096 0.548 0.000	
3_156 0_049 0_098 0_903 0_000	
3.200 0.050 0.100 1.314 0.000	
3.244 0.051 0.102 1.773 0.000 3.289 0.051 0.104 2.276 0.000	
3.289 0.051 0.104 2.276 0.000 3.333 0.052 0.107 2.819 0.000	
3.378 0.052 0.109 3.399 0.000	

3.422 3.467 3.511 3.556 3.600 3.644 3.689 3.733 3.778 3.822 3.867 3.911 3.956	0.053 0.054 0.055 0.055 0.056 0.057 0.057 0.058 0.059 0.059 0.060 0.061	0.111 0.114 0.116 0.119 0.121 0.124 0.126 0.129 0.131 0.134 0.136 0.139 0.142	4.015 4.665 5.345 6.057 6.797 7.565 8.360 9.182 10.03 10.90 11.79 12.71 13.65	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000

Flow Frequency Retu	urn Periods for Predeveloped
Return Period	Flow(cfs)
2 year	0.011005
5 year	0.018461
10 year	0.024053
25 year	0.031755
50 year	0.037907
100 year	0.044381

Flow Frequency	Return Periods for Developed Unmitigated
Return Period	Flow(cfs)
2 year	0.031765
5 year	0.054502
10 year	0.074008
25 year	0.104465
50 year	0.131866
100 year	0_16374

Flow Frequency	Return	Periods	for	Developed	Mitigated
Return Period		Flow (cfs	3)	_	- ,
2 year		0.0057	798		
5 year		0.0086	517		
10 year		0.0109	927		
25 year		0.0144	117		
50 year		0.0174	177		
100 year		0.0209	973		

Yearly	Peaks for Predevel	oped and Developed-Mitigated
Year	Predeveloped	Developed
1949	0.015	0.005
1950	0.013	Q.006
1951	0.027	0.026
1952	0.006	0.004
1953	0.008	0.006
1954	0.010	0.005
1955	0.009	0.004
1956	0.017	0.006
1957	0.007	0.005
1958	0.007	0.004
1959	0.010	0.005
1960	0.047	0.010
1961	0.014	0.015
1962	0.004	0.004
1963	0.032	0.006
1964	001.3	0.006
1965	0.012	0.006
1966	0.030	0.005
1967	0.015	0.005
1968	0.007	0.005
1969	0 009	0 005

1970	0.006	0.006
1971	0.010	0.006
1972	0.017	0.007
1973	0.006	0.006
1974	0.021	0.005
1975	0.012	0.006
1976	0.013	0.006
1977	0.002	0.005
1978	0.025	Q.006
1979	0.014	0.005
1980	0.018	0.015
1981	0.010	0.006
1982	0.015	0.015
1983	0.008	0.005
1984	0.004	0.005
1985	0.006	0.005
1986	0.012	0.005
1987	0.028	0.030
1988	0.008	0.005
1989	0.007	0.005
1990	0.015	0.007
1991	0.013	0.006
1992	0.008	0.006
1993	0.016	0.005
1994	0.005	0.004
1995	0.004	0.005
1996	0.014	0.007

Ranked	Yearly Peaks for	Predeveloped and Developed-Mitigated
Rank	Predeveloped	Developed
4	0 0010	

Rank	Predeveloped	Develope
1	0.0319	0.0258
2 3	0.0303	0.0154
3	0.0282	0.0153
4	0.0265	0.0146
5	0.0252	0.0104
6	0.0213	0.0067
7	0.0179	0.0066
8	0.0172	0.0065
9	0.0170	0.0062
10	0.0159	0.0059
11	0.0151	0.0059
12	0.0151	0.0059
13	0.0149	0.0058
14	0.0147	0.0057
15	0.0144	0.0057
16	0.0139	0.0057
17	0.0136	0.0056
18	0.0134	0.0056
19	0.0132	0.0056
20	0.0129	0.0056
21	0.0126	0.0055
22	0.0122	0.0055
23	0.0119	0.0055
24	0.0119	0.0055
25	0.0102	0.0054
26	0.0096	0.0054
27	0.0095	0.0054
28	0.0095	0.0053
29	0.0092	0.0053
30	0.0087	0.0053
31	0.0084	0.0052
32	0.0081	0.0052
33	0.0080	0.0051
34	0.0076	0.0051
35	0.0074	0.0051
36	0.0072	0-0049
37 38	0.0071	0.0049
	0.0066	0.0048
39 40	0.0065	0.0048
	0.0065	0.0047
41	0.0064	0.0047

42	0.0056	0.0046
43	0.0048	0.0042
44	0.0041	0.0042
45	0.0038	0.0042
46	0.0036	0.0040
47	0.0019	0.0037

				······································
1/2 2				
1/2 2 yes				
Flow (CFS)		Final	Percentage	Pass/Fail
0.0055	4173	3946	94.0	Pass
0.0058	3628	2059	56.0	Pass
0.0062	3164	1386	43.0	Pass
0.0065	2776	923	33.0	Pass
0.0068	2463	482	19.0	Pass
0.0071	2201	306	13.0	Pass
0.0075	1991	290	14.0	Pass
0.0078	1805	282	15.0	Pass
0.0081	1618	266	16.0	Pass
0.0084	1456	251	17.0	Pass
0.0088	1310	226	17.0	Pass
0.0091	1173	202	17.0	Pass
0.0094	1054	194	18.0	Pass
0.0098	937	185	19.0	Pass
0.0101	843	175	20.0	Pass
0.0104	746	165	22.0	Pass
0.0107	670	155	23.0	Pass
0.0111	603	143	23.0	Pass
0.0114	543	133	24.0	Pass
0.0117	480	122	25.0	Pass
0.0120	434	116	26.0	Pass
0.0124	378	107	28.0	Pass
0.0127	332	98	29.0	Pass
0.0130	293	88	30.0	Pass
0.0134	263	83	31.0	Pass
0.0137	236	77	32.0	
0.0140	210	71	33.0	Pass
0.0143	184	65	35.0	Pass
0.0147	171	56	32.0	Pass
0.0150	158	51	32.0	Pass
0.0153	143	48	33.0	Pass
0.0156	129	45	33.0	Pass
0.0160	120	44	34.0	Pass
0.0163	114	42	36.0	Pass
0.0166	105		36.0	Pass
0.0170	95	40	38.0	Pass
0.0173		40°	42.0	Pass
0.0176	89	38	42.0	Pass
	80	36	45.0	Pass
0.0179 0.0183	71 65	36	50.0	Pass
	65	34	52.0	Pass
0.0186 0.0189	60 5.6	32	53.0	Pass
	56	31	55.0	Pass
0.0192	50	2.9	58.0	Pass
0.0196	47	29	61.0	Pass
0.0199	46	27	58.0	Pass
0.0202	42	26	61.0	Pass
0.0206	39	25	64.0	Pass
0.0209	36	24	66.0	Pass
0.0212	34	23	67.0	Pass
0.0215	31.	22	70.0	Pass
0.0219	29	21	72.0	Pass
0.0222	26	19	73.0	Pass
0.0225	24	18	75.0	Pass
0.0229	23	16	69.0	Pass
0.0232	22	16	72.0	Pass
0.0235	18	14	77.0	Pass
0.0238	17	13	76.0	Pass
0.0242	14	11	78.0	Pass
0.0245	12	10	83.0	Pass
0.0248	10	9	90.0	Pass
0.0251	10	8	80.0	Pass
0.0255	8	8	100.0	Pass

0.0258 0.0261 0.0265 0.0268 0.0271 0.0274 0.0278 0.0281 0.0284 0.0297 0.0291 0.0294 0.0297 0.0301 0.0314 0.0317 0.0317 0.0320 0.0317 0.0323 0.0327 0.0333 0.0337 0.0340 0.0350 0.0350 0.0350 0.0350 0.0359 0.0366 0.0379 0.0379	87765554333332222211111111111111111111111111	66554443332221000000000000000000000000000000	75.0 85.0 71.0 83.0 80.0 80.0 75.0 100.0 66.0 66.0 66.0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0	PPPPPPPPPPPPPPPPPPPPPPPPPPPPPPPPPPPPPP
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Water Quality BMP Flow and Volume.

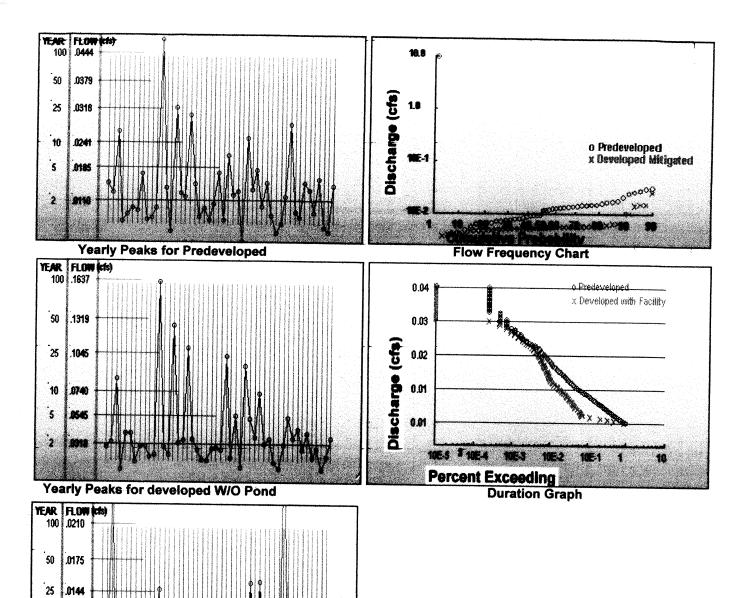
1002 CF / 21780 SF = 0.046 CF/SF -> 0.002 cy/SF On-line facility volume: 0.023 acre-feet

On-line facility target flow: 0.01 cfs. Adjusted for 15 min: 0.01 cfs.

Off-line facility target flow: 0 cfs.

Adjusted for 15 min: 0 cfs.

program and accompanying documentation as provided 'as-is' without warranty of any kind. The entire risk regarding the performance and results of this program is assumed by the user. AQUA TERRA Consultants and the Washington State Department of Ecology disclaims all warranties, either expressed or implied, including but not limited to implied warranties of program and accompanying documentation. In no event shall AQUA TERRA Consultants and/or the Washington State Department of Ecology be liable for any damages whatsoever (including without limitation to damages for loss of business profits, loss of business information, business interruption, and the like) arising out of the user of, or inability to use this program even if AQUA TERRA Consultants or the Washington State Department of Ecology has been advised of the possibility of such damages.



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2

Yearly Peaks for Developed W/Pond

APPENDIX D

WWHM Output for Parking Lot Designs

Project Name: Parking(open pond)

Site Address:

City :

Report Date : 7/27/2004
Gage : McMillian

Data Start : 1948 **Data End** : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

Basin

Basin : Pre-Dev
Flows To : Point of Compliance

GroundWater: No

Land Use Acres TILL FOREST: 0.519

DEVELOPED LAND USE

Basin : Basin 1 Flows To : Pond 1 GroundWater: No

Land Use Acres IMPERVIOUS: 0.519

RCHRES (POND) INFORMATION

Pond Name: Pond 1
Pond Type: Trapezoidal Pond Pond Flows to : Point of Compliance Pond Rain / Evep is not activated.

Dimensions

Depth: 5ft. Bottom Length: 71.02ft.
Bottom Width: 23.68ft.
Side slope 1: 3 To 1 Side slope 2: 3 To 1 Side slope 3: 3 To 1 Side slope 4: 3 To 1

Volume at Riser Head: 0.276 acre-ft. 12023 CF → 445 W Discharge Structure

Riser Height: 4 ft. Riser Diameter: 18 in. NotchType : Rectangular Notch Width: 0.010 ft. Notch Height: 0.851 ft.

Orifice 1 Diameter: 0.344 in. Elevation: 0 ft.

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt(cfs)
0.000	0.039	0.000	0.000	0.000
0.056	0.039	0.002	0.001	0.000
0.111	0.040	0.004	0.001	
0.167	0.041	0.007	0.001	0.000
0.222	0.042	0.009	0.001	0.000

		·		
0.278	0.042	0.011	0.002	0.000
0.333	0.043	0.014	0.002	0.000
0.389 0.444	0.044 0.045	0.016 0.018	0.002 0.002	0.000
0.500	0.045	0.021	0.002	0.000
0.556 0.611	0.046 0.047	0.024	0.002	0.000
0.667	0.047	0.026 0.029	0.002 0.003	0.000
0.722	0.048	0.031	0.003	0.000
0.778 0.833	0.049 0.050	0.034 0.037	0.003 0.003	0.000
0,889	0.051	0.040	0.003	0.000
0.944 1.000	0.052 0.052	0.043 0.045	0.003 0.003	0.000
1.056	0-053	0.048	0.003	0-000
1.111 1.167	0.054 0.055	0.051 0.054	0.003 0.003	0.000
1.222	0.056	0.057	0.003	0.000
1.278 1.333	0.057 0.057	0.061 0.064	0.004 0.004	0.000
1.389	0.058	0.067	0.004	0.000
1.444	0.059 0.060	0.070 0.074	0.004	0.000
1.556	0.061	0.077	0.004	0.000
1.611 1.667	0.062 0.063	0.080 0.084	0.004	0.000
1.722	0.064	0.087	0.004 0.004	0.000
1.778 1.833	0.064 0.065	0.091 0.094	0.004	0.000
1.889	0.066	0.098	0.004 0.004	0.000
1.944 2.000	0.067 0.068	0.102	0.004	Q.000
2.056	0.069	0.106 0.109	0.004 0.004	0.000
2.111	0.070	0.113	0.005	0.000
2.167 2.222	0.071 0.072	0.117 0.121	0.005 0.005	0.000
2.278	0_073	0.125	0.005	0_000
2.333 2.389	0.074 0.074	0.129 0.133	0.005 0.005	0.000
2.444	0.075	0.137	0.005	0.000
2.500 2.556	0.076 0.077	0.142 0.146	0.005 0.005	0.000
2.611	0.078	0.150	0.005	0.000
2.667 2.722	0.079 0.080	0.155 0.159	0.005 0.005	0.000
2.778	0.081	0.163	0.005	0,000
2.833 2.889	0.082 0.083	0.168 0.173	0.005 0.005	0.000
2.944	0.084	0.177	0.005	0.000
3.000 3.056	0.085 0.086	0.182 0.187	0.005 0.005	0.000
3.111	0.087	0.192	0.005	0.000
3.167 3.222	0.088 0.089	0.196 0.201	0.006 0.006	0.000
3.278	0.090	0.206	0.007	0.000
3.333 3.389	0.091 0.092	0.211 0.216	0.008 0.009	0.000
3.444	0.093	0.222	0.011	0.000
3.500 3.556	0.094 0.095	0.227 0.232	0.012	0.000
3.611	0.096	0.237	0.015	0.000
3.667 3.722	0.098 0.099	0.243 0.248	0.017 0.019	0.000
3.778	0.100	0.254	0.021	0.000
3.833 3.889	0.101 0.102	0.259 0.265	0.022	0.000
3.944	0.102	0.271	0.024 0.026	0.000
4.000 4.056	0.104 0.105	0.276 0.282	0.028	0,000
4.111	0.105	0.282	0.219 0.569	0.000
4.167	0.107	0.294	1.022	0.000
4.222	0.108	0.300	1,558	0.000

4.278	0.110	0.306	2.167	0.000
4.333	0.111	0.312	2.840	0.000
4.389	0.112	0.318	3.571	0.000
4.444	0.113	0.325	4.357	0.000
4.500				
	0.114	0.331	5.193	0.000
4.556	0.115	0.337	6.078	0.000
4.611	0.116	0.344	7.007	0.000
4.667	0.117	0.350	7.980	0.000
4.722	0.119	0.357	8.995	0.000
4.778	0.120	0.363	10.05	0.000
4.833	0.121	0.370	11.14	0.000
4.889	0.122	0.377	12.27	0.000
4.944	0.123	0.384	13.44	0.000
5.000	0.124	0.391	14.64	0.000

rrow rreductor Ke	eturn Periods for Predevelop
Return Period	Flow(cfs)
2 year	Q.011445
5 year	0.0192
10 year	0.025015
25 year	0.033025
50 year	0.039423
100 year	0.046157

Flow Frequency Return Periods for Developed Unmitigated

Return Period	Flow(cfs)	
2 year	0.149474	
5 year	0.199532	
10 year	0.235019	
25 year	0.282615	
50 year	0.320127	
100 year	0_359442	

Flow Frequency Return Periods for Developed Mitigated Return Period Flow(cfs)

Return Period	Flow(cfs)
2 year	0.006273
5 year	0.010398
10 year	0.014078
25 year	0.02005
50 year	0.025631
100 year	0.032345

Yearly Peaks for Predeveloped and Developed-Mitigated Year Predeveloped Developed

Year	Predeveloped	Developed
1949	0.016	0.005
1950	0.013	Q.005
1951	0.028	0.024
1952	0.007	0.004
1953	0.008	0.015
1954	0.010	0.005
1955	0.009	0.004
1956	0.018	0.019
1957	0.007	0.005
1958	0.007	0.005
1959	0.010	0.005
1960	0.049	0.008
1961	0.014	0.024
1962	0.004	0.004
1963	0.033	0.005
1964	0.013	0.005
1965	0.012	0.005
1966	0.032	0.005
1967	0.015	0.005
1968	0.008	0.005
1060	0 010	Λ ΛΛΕ

0.007	0.006
0.011	0.005
0.018	0.019
0.007	0.005
0.022	0.005
0.013	0.006
0.014	0.006
0.002	0.005
0.026	0.005
0.014	0.005
0.019	0.016
0.010	0.005
0.016	0.016
0.008	0.005
0.004	0.005
0.006	0.005
0.012	0.005
0.029	0.034
0.009	0.005
0.007	0.005
0.016	0.016
0.014	0.005
0.2008	0.005
0.017	0.005
0.005	0.004
0.004	0.005
0.015	0.012
	0.011 0.018 0.007 0.022 0.013 0.014 0.002 0.026 0.014 0.019 0.010 0.016 0.008 0.004 0.006 0.012 0.029 0.009 0.007 0.016 0.014 0.029 0.0100 0.015 0.017 0.005 0.004

Ranked Yearly Peaks for Predeveloped and Developed-Mitigated Rank Predeveloped Developed

1 0.0332 0.0240 2 0.0315 0.0237 3 0.0293 0.0194 4 0.0276 0.0192 5 0.0262 0.0164 6 0.0221 0.0155 7 0.0187 Q.0155 8 0.0179 0.0148 9 0.0177 0.0121 10 0.0165 0.0076 11 0.0157 0.0060 12 0.0157 0.0057 13 0.0155 0.0056 14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0055 17 0.0141 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0124 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 <td< th=""><th>Rank</th><th>Predeveloped</th><th>Developed</th></td<>	Rank	Predeveloped	Developed
4 0.0276 0.0192 5 0.0262 0.0164 6 0.0221 0.0155 7 0.0187 0.0155 8 0.0179 0.0148 9 0.0177 0.0121 10 0.0165 0.0076 11 0.0157 0.0060 12 0.0157 0.0057 13 0.0155 0.0056 14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0055 17 0.0141 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0053 29 0.0096 0.0052	1		0.0240
4 0.0276 0.0192 5 0.0262 0.0164 6 0.0221 0.0155 7 0.0187 0.0155 8 0.0179 0.0148 9 0.0177 0.0121 10 0.0165 0.0076 11 0.0157 0.0060 12 0.0157 0.0057 13 0.0155 0.0056 14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0055 17 0.0141 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0053 29 0.0096 0.0052	2		0.0237
5 0.0262 0.0164 6 0.0221 0.0155 7 0.0187 0.0155 8 0.0179 0.0148 9 0.0177 0.0121 10 0.0165 0.0076 11 0.0157 0.0060 12 0.0157 0.0057 13 0.0155 0.0056 14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0053 29 0.0096 0.0053 30 0.0091 0.0052 31 0.0087 0.0050	3		0.0194
6 0.0221 0.0155 7 0.0187 0.0155 8 0.0179 0.0148 9 0.0177 0.0121 10 0.0165 0.0076 11 0.0157 0.0060 12 0.0157 0.0057 13 0.0155 0.0056 14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0050 32 0.0084 0.0050	4	0.0276	0.0192
7 0.0187 Q.0155 8 0.0179 0.0148 9 0.0177 0.0121 10 0.0165 0.0076 11 0.0157 0.0060 12 0.0157 0.0057 13 0.0155 0.0056 14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0055 17 0.0141 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0053 29 0.0096 0.0052 31 0.0087 0.0052 31 0.008			0.0164
8 0.0179 0.0148 9 0.0177 0.0121 10 0.0165 0.0076 11 0.0157 0.0060 12 0.0157 0.0057 13 0.0155 0.0056 14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0050 32 0.0084 0.0050 34 0.0079 0.0049 35 0.0077 0.0049			0.0155
9 0.0177 0.0121 10 0.0165 0.0076 11 0.0157 0.0060 12 0.0157 0.0057 13 0.0155 0.0056 14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 34 0.0079 0.0049 35 0.0077 0.0049		0.0187	Q.0155
10 0.0165 0.0076 11 0.0157 0.0060 12 0.0157 0.0057 13 0.0155 0.0056 14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048		0.0179	0.0148
11 0.0157 0.0060 12 0.0157 0.0057 13 0.0155 0.0056 14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0055 17 0.0141 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0074 0.0048		0.0177	0.0121
12 0.0157 0.0057 13 0.0155 0.0056 14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0055 17 0.0141 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0053 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0074 0.0048 37 0.0049 0.0048		0.0165	0.0076
13 0.0155 0.0056 14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0054 17 0.0141 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0067 0.0047		0.0157	0.0060
14 0.0153 0.0055 15 0.0149 0.0055 16 0.0145 0.0055 17 0.0141 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0053 29 0.0099 0.0053 30 0.0091 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0069 0.0048 39 0.0067 0.0047		0.0157	0.0057
15 0.0149 0.0055 16 0.0145 0.0055 17 0.0141 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047 <td></td> <td>0.0155</td> <td>0.0056</td>		0.0155	0.0056
16 0.0145 0.0055 17 0.0141 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0047 39 0.0067 0.0047 40 0.0067 0.0047 <td></td> <td>0-0153</td> <td>0_0055</td>		0-0153	0_0055
17 0.0141 0.0054 18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 39 0.0067 0.0047 40 0.0067 0.0047		0.0149	0.0055
18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 39 0.0067 0.0047 40 0.0067 0.0047 40 0.0067 0.0047		0.0145	0.0055
18 0.0140 0.0054 19 0.0137 0.0054 20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047	17	0.0141	0.0054
20 0.0135 0.0054 21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 39 0.0067 0.0047 40 0.0067 0.0047		0.0140	
21 0.0132 0.0054 22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047		0.0137	0.0054
22 0.0127 0.0054 23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047			0.0054
23 0.0124 0.0054 24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047		0.0132	0.0054
24 0.0124 0.0054 25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047			0.0054
25 0.0106 0.0054 26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047	23	0.0124	0,0054
26 0.0100 0.0054 27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047			
27 0.0099 0.0054 28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047			
28 0.0099 0.0053 29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047		0.0100	0.0054
29 0.0096 0.0052 30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047		0.0099	0.0054
30 0.0091 0.0052 31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047		0.0099	0.0053
31 0.0087 0.0051 32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047			
32 0.0084 0.0050 33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047		0.0091	0.0052
33 0.0083 0.0050 34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047			0.0051
34 0.0079 0.0049 35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047			0.0050
35 0.0077 0.0049 36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047			0.0050
36 0.0074 0.0048 37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047		0.0079	0.0049
37 0.0074 0.0048 38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047		0.0077	0.0049
38 0.0069 0.0048 39 0.0067 0.0047 40 0.0067 0.0047			0.0048
39 0.0067 0.0047 40 0.0067 0.0047			0.0048
40 0.0067 0.0047			0.0048
40 0.0067 0.0047	39	0.0067	0.0047
0.0067 0.0046	40	0.0067	
	41	0.0067	0.0046

42	0.0059	0.0045
43	0.0050	0.0045
44	0.0043	0.0043
45	0.0040	0.0043
46	0.0038	0.0041
47	0.0020	0.0039

47	0.0020		0.003	
1/2 2 yes				
Flow (CFS)		Final	Percentage	Pass/Fail
0.0057	4174	1926	46.0	Pass
0.0061	3628	1740	47.0	Pass
0.0064	3165	1592	50.0	Pass
0.0067	2776	1478	53.0	Pass
0.0071	2463	1324	53.0	Pass
0.0074	2202	1227	55.0	Pass
0.0078 0.0081	1991	1140	57.0	Pass
0.0084	1805 1620	1060 1001	58.0	Pass
0.0088	1456	936	61.0 64.0	Pass
0.0091	1310	879	67.0	Pass Pass
0.0095	1173	816	69.0	Pass
0.0098	1054	759	72.0	Pass
0.0101	938	703	74.0	Pass
0.0105	843	641	76.0	Pass
0.0108	747	592	79.0	Pass
0.0112	670	535	79.0	Pass
0.0115	603	494	81.0	Pass
0.0118	545	450	82.0	Pass
0.0122	480	405	84.0	Pass
0.0125	432	376	87.0	Pass
0.0129 0.0132	378	343	90.0	Pass
0.0132	332 293	310 276	93.0	Pass
0.0130	263	246	94.0 93.0	Pass
0.0142	236	214	90.0	Pāss Pass
0.0146	210	186	88-0	Pass
0.0149	184	163	88.0	Pass
0.0153	171	146	85.0	Pass
0.0156	158	126	79.0	Pass
0.0159	143	117	81.0	Pass
0.0163	129	105	81.0	Pass
0.0166	120	97	80.0	Pass
0.0170	114	91	79.0	Pass
0.0173	106	85	80.0	Pass
0.0176	95	82	86.0	Pass
0.0180 0.0183	89 80	76 70	85.0	Pass
0.0187	72	70 65	87.0 90.0	Pass
0.0190	65	60	92.0	Pass Pass
0.0193	60	51	85.0	Pass
0.0197	56	47	83.0	Pass
0.0200	50	4.6	92.0	Pass
0.0204	47	43	91.0	Pass
0.0207	46	39	84.0	Pass
0.0210	42	38	90.0	Pass
0.0214	39	33	84.0	Pass
0.0217	36	30	83.0	Pass
0.0221	34	27	79.0	Pass
0.0224	31	24	77.0	Pass
0.0227 0.0231	29 26	23 19	79.0 73.0	Pass
0.0231	24	19 17	70.0	Pass Pass
0.0234	23	12	52.0	Pass
0.0241	22	9	40.0	Pass
0.0244	18	8	44.0	Pass
0.0248	17	8	47.0	Pass
0.0251	14	7	50.0	Pass
0.0255	12	7	58.0	Pass
0.0258	10	6	60.0	Pass
0.0261	10	5	50.0	Pass
0.0265	8	5	62.0	Pagg

0.0268 0.0272 0.0275 0.0278 0.0282 0.0285 0.0289 0.0299 0.0299 0.0302 0.0306 0.0309 0.0313 0.0316 0.0319 0.0323 0.0326 0.0330 0.0333 0.0340 0.0340 0.0350 0.0353 0.0357 0.0360 0.0364 0.0377 0.0367 0.0374 0.0377 0.0374 0.0377 0.0384 0.0384 0.0394	8 7 7 6 5 5 5 5 4 3 3 3 3 3 3 2 2 2 2 2 2 1 1 1 1 1 1 1 1	4 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	50.0 57.0 42.0 33.0 40.0 40.0 50.0 66.0 66.0 66.0 66.0 100.0	SSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSS
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Water Quality BMP Flow and Volume.

On-line facility volume: 0.019 acre-feet

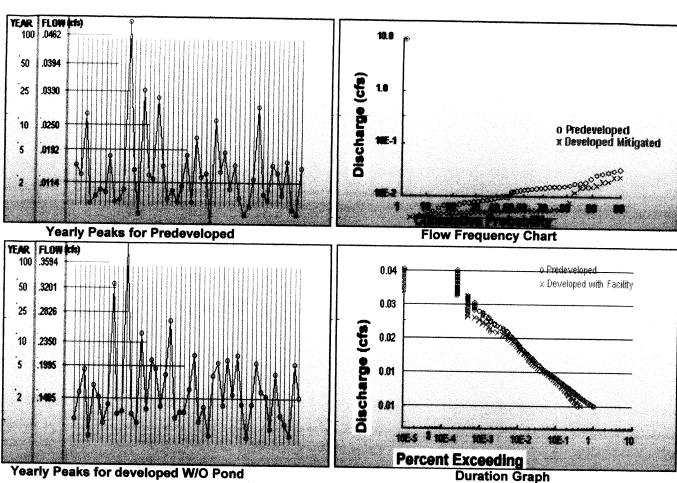
On-line facility target flow: 0.01 cfs. Adjusted for 15 min: 0.01 cfs.

Off-line facility target flow: 0 cfs.

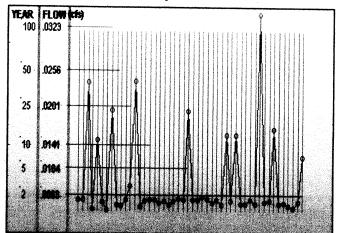
Adjusted for 15 min: 0 ofs.

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828 cf -> 31 cm



Yearly Peaks for developed W/O Pond



Yearly Peaks for Developed W/Pond

Project Name: Parking(vault)

Site Address:

City :

Report Date: 7/27/2004 Gage : McMillian Data Start : 1948

Data End : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

: Pre-Dev

Flows To : Point of Compliance

GroundWater: No

Land Use

Acres

TILL FOREST:

0.459

DEVELOPED LAND USE

Basin : Basin 1 Flows To : Pond 1 GroundWater: No

Land Use

Acres

IMPERVIOUS: 0.459

RCHRES (POND) INFORMATION Pond Name: Pond 1
Pond Type: Trapezoidal Pond

Pond Flows to : Point of Compliance

Pond Rain / Evap is not activated.

Dimensions

Depth: 5ft. Bottom Length: 65.5ft. Bottom Width: 21.86ft. Side slope 1: 3 To 1 Side slope 2: 3 To 1
Side slope 3: 3 To 1
Side slope 4: 3 To 1

Volume at Riser Head: 0.245 acre-ft. 10,672 CF

Discharge Structure Riser Height: 4 ft. Riser Diameter: 18 in.

NotchType : Rectangular Notch Width: 0_010 ft. Notch Height: 0.811 ft.

Orifice 1 Diameter: 0.321 in. Elevation: 0 ft.

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt(cfs)
0.000	0.033	0.000	0.000	0.000
0.056	0.034	0.002	0.001	0.000
0.111	0.034	0.004	0.001	0.000
0.167	0.035	0.006	0.001	0.000
0 222	0 036	0 008	0 001	0 000

0.3339 0.4400 0.55617 0.66228339 0.6777339 0.0000 0.0000 0.0000 0.0000 0.0000 0.	0.036 0.037 0.038 0.038 0.038 0.039 0.041 0.041 0.042 0.043 0.044 0.045 0.046 0.046 0.046 0.046 0.047 0.046 0.046 0.050 0.051 0.053 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.066 0.065 0.066 0.066 0.066 0.067 0.068 0.070 0.075 0.075 0.077 0.075 0.077 0.075 0.077 0.081 0.083 0.084 0.085 0.087 0.088 0.088 0.088	0.010 0.012 0.014 0.016 0.018 0.020 0.022 0.025 0.027 0.029 0.032 0.034 0.037 0.039 0.044 0.047 0.050 0.050 0.055 0.055 0.058 0.067 0.073 0.079 0.079 0.089 0.099 0.099 0.099 0.099 0.099 0.109 0.113 0.117 0.124 0.124 0.132 0.144 0.148 0.156 0.164 0.148 0.156 0.164 0.169 0.113 0.144 0.148 0.156 0.164 0.169 0.173 0.144 0.148 0.156 0.164 0.169 0.173 0.178 0.164 0.164 0.173 0.178 0.164 0.164 0.173 0.178 0.164 0.164 0.178 0.178 0.199 0.199 0.109 0.201 0.	0.001 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.004 0.005	0.000 0.000	
3.444 3.500 3.556 3.611	0.084 0.085 0.086 0.087	0.196 0.201 0.205 0.210	0.009 0.010 0.012 0.014	0.000 0.000 0.000	
3.667 3.722 3.778 3.833 3.889	0.088 0.089 0.090 0.091 0.092	0.215 0.220 0.225 0.230 0.235	0.015 0.017 0.019 0.020	0.000 0.000 0.000 0.000	
3.944 4.000 4.056 4.111	0.093 0.094 0.095 0.096	0.240 0.245 0.251 0.256	0.022 0.024 0.026 0.217 0.567	0.000 0.000 0.000 0.000 0.000	
4.167 4.222	0.097 0.098	0.261 0.267	1.020 1.556	0.000 0.000	

4.278	0.099	0-272	2-165	0.000
4.333	0.101	0.278	2.837	0.000
4.389	0.102	0.283	3.569	0.000
4.444	0.103	0.289	4.355	0.000
4.500	0.104	0.295	5.191	0.000
4.556	0.105	0.301	6.075	0.000
4.611	0.106	0.307	7.005	0.000
4.667	0.107	0.312	7.978	0.000
4.722	0.108	0.318	8.993	0.000
4.778	0.109	0.324	10.05	0.000
4.833	0.110	0.331	11.14	0.000
4.889	0.111	0.337	12.27	0.000
4.944	0.113	0.343	13.43	0.000
5.000	0.114	0.349	14.63	0.000

Flow Frequency Return Return Period	n Periods for Predeveloped Flow(cfs)
2 year	0.010125
5 year	0.016984
10 year	0.022129
25 year	0.029215
50 year	0.034874
100 year	0.040831

Flow Frequency Retur	n Periods for Developed Unmitigated
Return Period	Flow(cfs)
2 year	0.132227
5 year	0.176509
10 year	0.207901
25 year	0.250005
50 year	0.283189
100 year	0_317968

Flow Frequency	Return	Periods	for	Developed	Mitigated
Return Period		Flow (cfs	3)		- ,
2 year		0.0055	515		
5 year		0.0092	23		
10 year		0.0125	69		
25 year		0.0180	21		
50 year		0.0231	4.5		
100 year		0.0293	337		

Yearly	Peaks	for Predevelor	ped and Developed-Mitigated
Year		Predeveloped	Developed
1949		0.014	0.005
1950		0.012	Q.005
1951		0.024	0.022
1952		0.006	0.004
1953		0.007	0.013
1954		0.009	0.004
1955		0.008	0.003
1956		0.016	0.018
1957		0.006	0.004
1958		0.007	0.004
1959		0.009	0.005
1960		0.044	0.006
1961		0.013	0.022
1962		0.004	0.004
1963		0.029	0.005
1964		0-012	0.005
1965		0.011	0.005
1966		0.028	0.004
1967		0.014	0.005
1968		0.007	0.004
1060		0 000	0 005

1970 1971 1972 1973 1974 1975 1976 1977 1978 1979 1980 1981 1982 1983 1984 1985 1986 1987	0.006 0.009 0.016 0.006 0.020 0.011 0.012 0.002 0.023 0.012 0.017 0.009 0.014 0.007 0.003 0.003 0.005 0.011 0.026 0.008	0.005 0.005 0.018 0.005 0.005 0.005 0.004 0.005 0.014 0.005 0.014 0.004 0.004 0.004
1987	0.026	0.029
1988 1989 1990	0.008 0.007 0.014	0.005 0.005 0.015
1991 1992	0.012	0.004 0-004
1993 1994 1995	0.015 0.004 0.004	0.004 0.004 0.005
1996	0.013	0.003

Ranked Yearly Peaks for Predeveloped and Developed-Mitigated Rank Predeveloped Developed

Rank	Predeveloped	Develope
1	0.0294	0.0220
-2	0.0279	0.0219
3	0.0259	0.0180
4	0.0244	0.0178
5	0.0232	0.0147
6	0.0196	0.0141
7	0.0165	0.0140
8	0.0159	0.0133
9	0.0157	0.0109
10	0.0146	0.0064
11	0.0139	0.0052
12	0.0138	0.0049
13	0.0137	0.0049
14	0_0136	0-0048
15	0.0132	0.0048
16	0.0128	0.0048
17	0.0125	0.0048
18	0.0123	0.0048
19	0.0121	0.0048
20	0.0119	0.0047
21	0.0116	0.0047
22	0.0113	0.0047
23	0.0110	0.0047
24	0.0109	0.0047
25	0.0094	0.0047
26	0.0089	0.0047
27	0.0088	0.0047
28	0.0087	0.0046
29	0.0085	0.0046
30	0.0080	0.0045
31	0.0077	0.0045
32	0.0074	0.0044
33	0.0073	0.0043
34	0.0070	0.0043
35	0.0068	0.0043
36	0_0066	0.0042
37	0.0065	0.0042
38	0.0061	0.0042
39	0.0060	0.0041
40	0.0059	0.0041
41	0.0059	0.0040

42	0_0052	0_0040
43	0.0045	0.0040
44	0.0038	0.0038
45	0.0035	0.0038
46	0.0034	0.0036
47	0.0017	0.0034

1/2 2 yea	r to 50	year			
Flow (CFS)	Predev	Final	Percentage	Pass/Fail	
0.0051	4173	1821	43.0	Pass	
0.0054	3628	1679	46.0	Pass	
0.0057	3165	1540	48.0	Pass	
0.0060	2776	1406	50.0	Pass	
0.0063	2462	1283	52.0	Pass	
0.0066 0.0069	2201 1991	1189 1114	54.0 55.0	Pass Pass	
0.0072	1805	1040	57.0	Pass	
0.0075	1618	980	60.0	Pass	
0.0078	1456	915	62.0	Pass	
0.0081	1310	866	66.0	Pass	
0.0084	1173	810	69.0	Pass	
0.0087	1054	751	71.0	Pass	
0.0090 0.0093	937 841	6 98 640	74.0 76.0	Pass	
0.0096	746	583	78.0	Pass Pass	
0.0099	667	541	81.0	Pass	
0.0102	602	496	82.0	Pass	
0.0105	543	453	83.0	Pass	
0.0108	480	423	88.0	Pass	
0_0111	434	382	88_0	Pass	
0.0114	378	350	92.0	Pass	
0.0117 0.0120	332 293	322 289	96.0 98.0	Pass	
0.0123	263	259	98.0	Pass Pass	
0.0126	236	232	98.0	Pass	
0.0129	209	201	96.0	Pass	
0.0132	184	186	101.0	Pass	
0.0135	171	160	93.0	Pass	
0.0138	158	146	92.0	Pass	
0.0141	143	126	88.0	Pass	
0.0144	129	114	88.0	Pass	
0.0147 0.0150	120 115	102 96	85.0 83.0	Pass Pass	
0.0153	105	92	87.0	Pass	
0.0156	95	86	90.0	Pass	
0.0159	89	80	89.0	Pass	
0.0162	80	76	95.0	Pass	
0.0165	72	73	101.0	Pass	
0.0168	65	67	103.0	Pass	
0.0171 0.0174	60 56	63	104.0	Pass	
0.0174	56 50	60 53	107.0 105.0	Pass Pass	
0.0180	47	46	97.0	Pass	
0.0183	46	44	95.0	Pass	
0.0186	42	41	97.0	Pass	
0.0189	39	39	100.0	Pass	
0.0192	36	37	102.0	Pass	
0.0195	34	34	100.0	Pass	
0.0198 0.0201	31 29	30 28	96.0 96.0	Pass Pass	
0.0201	26	24	92.0	Pass	
0.0207	24	24	100.0	Pass	
0.0210	23	20	86.0	Pass	
0.0213	22	18	81.0	Pass	
0.0216	18	16	88.0	Pass	
0.0219	17	10	58.0	Pass	
0.0222	14	8	57.0	Pass	
0.0225	12	8 7	66.0	Pass	
0.0228 0.0231	10 10	7	70.0 70.0	Pass Pass	
0.0231	8	6	75.0	ræss Pass	
	-	.,			

0.0237 0.0240 0.0243 0.0246 0.0249 0.0252 0.0255 0.0258 0.0261 0.0264 0.0267 0.0270 0.0273 0.0276 0.0279 0.0286 0.0289 0.0292 0.0292 0.0295 0.0298 0.0301 0.0301 0.0301 0.0313 0.0316 0.0319 0.0319 0.0322 0.0328 0.0319 0.0328 0.0331 0.0334 0.0337 0.0340 0.0349	87765554333332222211111111111111111111111111	65533222222222100000000000000000000000000	75.0 71.0 71.0 50.0 60.0 40.0 50.0 66.0 66.0 66.0 66.0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0	Passssssssssssssssssssssssssssssssssss
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Water Quality BMP Flow and Volume.

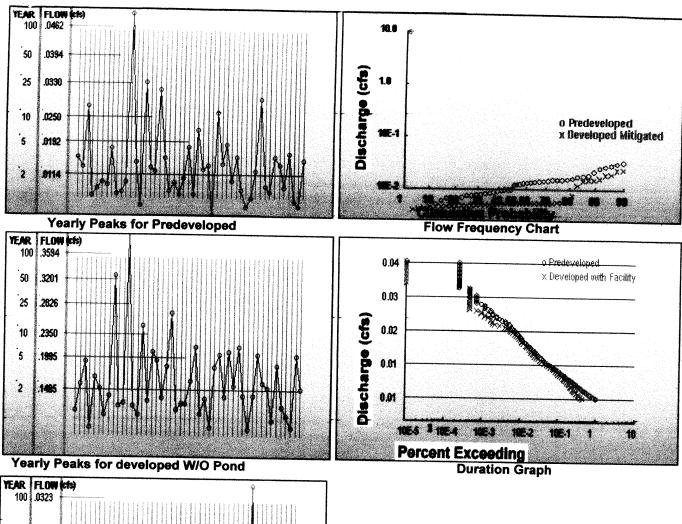
On-line facility volume: 0.019 acre-feet -> 828 CF

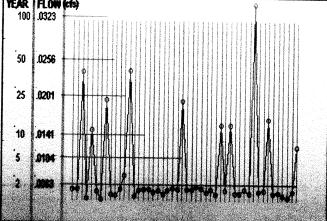
On-line facility target flow: 0.01 cfs.

Adjusted for 15 min: 0.01 cfs. Off-line facility target flow: 0 cfs.

Adjusted for 15 min: 0 cfs.

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Yearly Peaks for Developed W/Pond

Project Name: parking(LID_NO_INF)

Site Address:

City :

Report Date: 6/9/2004

Gage : McMillian
Data Start : 1948
Data End : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

Basin : Pre-Dev

Flows To : Point of Compliance

GroundWater: No

Land Use

Land Use Acres
TILL FOREST: 0.459

DEVELOPED LAND USE

Basin : Basin 1 Flows To : F_Table GroundWater: No

Land Use

Acres

IMPERVIOUS:

0.459

RCHRES (POND) INFORMATION Pond Name: F_Table
Pond Type: Table

Pond Flows to : Point of Compliance

Pond Rain / Evap is not activated.

Dimensions

Depth:

Oft.

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt(cfs)
0.000	0.000	0.000	0.000	0.000
0.130	0.459	0.018	0.002	0.000
0.260	0.459	0.036	0.002	0.000
0.390	0.459	0.054	0.003	0.000
0.520	0.459	0.072	0.003	0.000
0.650	0.459	0.090	0.004	0.000
0.780	0.459	0.107	0.004	0.000
0.910	0.459	0.125	0.004	0.000
1.040	0.459	0.143	0.004	0.000
1.170	0.459	0.161	0.005	
1.300	0.459	0.179	0.005	0.000
1.430	0.459	0.197	0.007	0.000
1.560	0.459	0.215	0.008	0.000
1.690	0.459	0.233	0.016	0.000
1.820	0.459	0.251	0.021	0.000
1.950	0.459	0.269	0.035	0.000
2.080	0.459	0.287	0.539	0.000
2.210	0.459	0.304	1.398	
2.340	0.459	0.322		0.000
2 470	0.459	0.322	2.426	0.000
		11 3711	9 700	0 000

2.600 2.730 2.860 2.990 3.120 3.380 3.510 3.640 3.770 3.900 4.160 4.290 4.550 4.680 4.940 5.200 5.330 5.590 5.330 5.590 5.720 5.850 6.110 6.630 6.630 6.760 7.020 7.150 7.280 7.150 7.280 7.150 7.280 7.150 7.280 7.290 7.280 7.280 7.290 7.280 7.290 7.200	0.459 0.459	0.358 0.376 0.394 0.412 0.430 0.448 0.466 0.484 0.501 0.519 0.555 0.573 0.627 0.645 0.663 0.680 0.716 0.734 0.752 0.770 0.788 0.806 0.824 0.842 0.860 0.987 0.9895 1.003 1.021 1.039 1.057 1.044 1.128 1.146 1.128 1.146 1.128 1.146 1.128 1.146 1.128 1.146 1.128 1.146 1.128 1.146 1.128 1.146 1.128 1.146 1.128 1.146 1.128 1.146 1.129 1.128 1.146 1.128 1.146 1.146 1.146 1.146 1.146 1.152 1.164 1.178 1.182 1.199 1.199 1.109 1.110 1.128 1.146 1.146 1.157 1.147 1.148 1.146 1.157 1.147 1.148 1.146 1.157 1.148 1.148 1.146 1.157 1	3.112 3.403 3.671 3.920 4.155 4.377 4.589 4.791 4.595 5.351 5.526 5.859 6.174 6.325 6.617 7.168 7.299 7.428 7.554 7.679 7.801 7.921 8.040 8.157 8.273 8.386 8.498 8.609 8.719 8.933 9.143 9.348 9.449 9.548 9.647 9.745 9.842 9.745 9.842 9.745 9.842 9.745 9.937 10.13 10.22 10.31 10.49 10.587 10.676 10.884 11.69 11.77	0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
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11.96 12.09 12.22 12.35 12.48 12.61 12.74	0.459 0.459 0.459 0.459 0.459 0.459	1.647 1.665 1.683 1.701 1.719 1.737	12.09 12.17 12.24 12.32 12.40 12.47 12.55	0.000 0.000 0.000 0.000 0.000 0.000
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rrow rreduency	Return Periods for Predeveloped
Return Period	Flow(cfs)
2 year	0.010125
5 year	0.016984
10 year	0.022129
25 year	0.029215
50 year	0.034874
100 year	0.040831

100 year 0.034874
100 year 0.040831

Flow Frequency Return Periods for Developed Unmitigated Return Period

Return Period	Flow(cfs)
2 year	0.132227
5 year	0.176509
10 year	0.207901
25 year	0.250005
50 year	0.283189
100 year	0.317968

Flow Frequency Return Periods for Developed Mitigated
Return Period Flow(cfs)

Return Period	Flow(cfs)
2 year	0.005569
5 year	0.009136
10 year	0.012291
25 year	0.017376
50 year	0.022099
100 year	0.027753

Yearly Peaks for Predeveloped and Developed-Mitigated

		bed and ne.
Year	Predeveloped	Develope
1949	0.014	0.005
1950	0.012	0.005
1951	0.024	0.023
1952	0.006	0.003
1953	0.007	0.014
1954	0.009	0.005
1955	0.008	0.003
1956	0.016	0.017
1957	0.006	0.004
1958	0.007	0.004
1959	0.009	0.005
1960	0.044	0.006
1961	0.013	0.022
1962	0.004	0.004
1963	0.029	0.005
1964	0.012	0.006
1965	0.011	0.005
1966	0.028	0.004
1967	0.014	0.005
1968	0.007	0.004
1969	0.008	0.005
1970	0.006	0.006
1971	0.009	0.005
1972	0.016	0.017
1973	0.006	0.005
1974	0.020	0.005
1975	0.011	0.006
1976	0.012	0.006

1977	0.002	0.004
1978	0.023	0.005
1979	0.012	0.004
1980	0.017	0.012
1981	0.009	0.005
1982	0.014	0.013
1983	0.007	0.004
1984	0.003	0.004
1985	0.005	0.005
1986	0.011	0.004
1987	0.026	0.027
1988	0.008	0.005
1989	0.007	0.005
1990	0.014	0.014
1991	0.012	0.004
1992	0.007	0.004
1993	0.015	0.004
1994	0.004	0.004
1995	0.004	0.005
1996	0.013	0.008

Ranked Yearly Peaks for Predeveloped and Developed-Mitigated Rank Predeveloped Developed

Rank	Predeveloped	Developed
1	0.0294	0.0227
2	0.0279	0.0223
3	0.0259	0.0170
4	0.0244	0.0169
5	0.0232	0.0141
6	0.0196	0.0140
7	0.0165	0.0129
8	0.0159	0.0118
9	0.0157	0.0076
10	0.0146	0.0062
11	0.0139	0.0061
12	0.0138	0.0058
13	0.0137	0.0058
14	0.0136	0.0056
15	0.0132	0.0054
16	0.0128	0.0053
17	0.0125	0.0051
18	0.0123	0.0050
19	0.0121	0.0050
20	0.0119	0.0050
21	0.0116	0-0050
22	0.0113	0.0049
23	0.0110	0.0049
24	0.0109	0.0049
25	0.0094	0.0049
26	0.0089	0.0048
27	0.0088	0.0048
28	0.0087	0.0047
29	0.0085	0.0046
30	0.0080	0.0046
31	0.0077	0.0046
32	0.0074	0.0044
33	0.0073	0.0043
34	0.0070	0.0043
35	0.0068	0.0042
36	0.0066	0.0042
37	0.0065	0.0042
38	0.0061	0.0042
39	0.0060	0.0041
40	0.0059	0.0040
41	0.0059	0.0040
42	0.0052	0.0039
43	0.0045	0_0039
44	0.0038	0.0037
45	0.0035	0.0036
46	0.0034	0.0034
47	0.0017	0.0033

1/2 2 v	rear to 50	Vear		
Flow (CF	'S) Predev	Final		Pass/Fail
0.0051	4173	2850	68.0	Pass
0.0054 0.0057	3628 3165	2465	67.0	Pass
0.0060	2776	2136 1912	67.0 68.0	Pass
0.0063	2462	1735	70.0	Pass Pass
0.0066	2201	1533	69.0	Pass
0.0069	1991	1290	64.0	Pass
0.0072	1805	961	53.0	Pass
0.0075	1618	660	40.0	Pass
0.0078 0.0081	1456 1310	526	36.0	Pass
0.0084	1173	502 476	38.0 40.0	Pass
0.0087	1054	455	43.0	Pass Pass
0.0090	937	427	45.0	Pass
0.0093	841	396	47.0	Pass
0.0096 0.0099	746 667	367	49.0	Pass
0.0102	602	344 317	51.0 52.0	Pass
0.0105	543	298	54.0	Pass Pass
0.0108	480	282	58.0	Pass
0.0111	434	264	60.0	Pass
0.0114 0.0117	378	246	65.0	Pass
0.0117	332 293	220 195	66.0	Pass
0.0123	263	179	66.0 68.0	Pass
0.0126	236	165	69.0	Pass Pass
0.0129	209	150	71.0	Pass
0.0132	184	141	7 6 .0	Pass
0.0135 0.0138	171	122	71.0	Pass
0.0141	158 143	116 104	73.0 72.0	Pass
0.0144	129	97	75.0	Pass Pass
0.0147	120	92	76.0	Pass
0.0150	115	89	77.0	Pass
0.0153	105	86	81_0	Pass
0.0156 0.0159	95 89	82	86.0	Pass
0.0162	80	80 74	89.0 92.0	Pass
0.0165	72	68	94.0	Pass Pass
0.0168	65	62	95.0	Pass
0.0171	60	54	90.0	Pass
0.0174 0.0177	56 50	52	92.0	Pass
0.0180	47	50 4 7	100.0 100.0	Pass
0.0183	46	43	93.0	Pass Pass
0.0186	42	42	100.0	Pass
0.0189	39	38	97.0	Pass
0.0192 0.0195	36	35	97.0	Pass
0.0193	34 31	33 29	97.0	Pass
0.0201	29	25	93.0 86.0	Pass Pass
0.0204	26	23	88.0	Pass
0.0207	24	20	83.0	Pass
0.0210	23	17	73.0	Pass
0.0213 0.0216	22 18	14	63.0	Pass
0.0219	17	13 10	72.0 58.0	Pass
0.0222	14	8	57.0	Pass Pass
0.0225	12	7	58.0	Pass
0.0228	10	6	60.0	Pass
0.0231 0.0234	10	6	60.0	Pass
0.0234	8 8	5 5	62.0 62.0	Pass
0.0240	7	5	71.0	Pass Pass
0.0243	7	4	57.0	Pass
0.0246	6	3	50.0	Pass
0.0249	5	3	60.0	Pass
0.0252 0.0255	5 5	3 3	60.0	Pass
0.0200	<u> </u>	J	60.0	Pass

0.0258 4 2 0.0261 3 2 0.0264 3 2 0.0267 3 1 0.0270 3 0 0.0273 3 0 0.0276 3 0 0.0279 2 0 0.0282 2 0 0.0286 2 0 0.0299 2 0 0.0299 1 0 0.0301 1 0 0.0304 1 0 0.0310 1 0 0.0313 1 0 0.0316 1 0 0.0322 1 0 0.0328 1 0 0.0328 1 0 0.0331 1 0 0.0328 1 0 0.0334 1 0 0.0344 1 0 0.0346 1 0 0.0349 1 0	50.0 66.0 66.0 33.0 .0 .0 .0 .0 .0 .0 .0 .0 .0	Passss Pass Passs Passs Passs Passs Passs Passs Passs Passs Passs Passs Pass Passs Passs Passs Passs Passs Passs Passs Passs Passs Passs Passs Passs Passs Passs Passs Pass P
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Water Quality EMP Flow and Volume.

On-line facility volume: 0.008 acre-feet

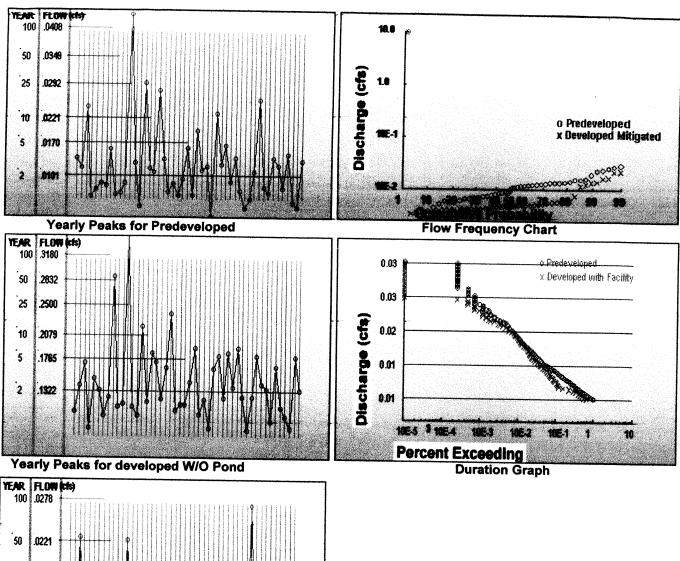
On-line facility target flow: 0 cfs.

Adjusted for 15 min: 0 cfs.

Off-line facility target flow: 0 cfs.

Adjusted for 15 min: 0 cfs.

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Yearly Peaks for Developed W/Pond

APPENDIX E

WWHM Output for Soil Rehabilitation

Project Name: landscape

Site Address:

City

Report Date : 6/10/2004 Gage : McMillian

Data Start : 1948 Data End : 1996 Precip Scale: 1.00

Pan Evap Factor entered by user: 0

PREDEVELOPED LAND USE

Basin

: Basin 1

Flows To : Point of Compliance

GroundWater: No

Land Use

TILL FOREST:

Acres

DEVELOPED LAND USE

Basin : Basin 1 Flows To : Pond 1 GroundWater: No

Land Use

TILL GRASS:

Acres

0.574

RCHRES (POND) INFORMATION

Pond Name: Pond 1
Pond Type: Trapezoidal Pond

Pond Flows to : Point of Compliance Pond Rain / Evap is not activated.

Dimensions

Depth:

5ft.

Bottom Length: 11.42ft. Bottom Width: 3.87ft.

Side slope 1: 3 To 1 Side slope 2: 3 To 1 Side slope 3: 3 To 1 Side slope 4: 3 To 1

Volume at Riser Head: 0.039 acre-ft. - 1699 CF

Discharge Structure Riser Height: 4 ft.

169.9 CF/ 2500 SF lamos scape

Riser Diameter: 18 in.

6.29 cy.

NotchType : Rectangular Notch Width: 0.011 ft.

Notch Height: 1.480 ft.

Orifice 1 Diameter: 0.643 in. Elevation: 0 ft.

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt(cfs)
0.000	0.001	0.000	0.000	0.000
0.056	0.001	0.000	0.003	0.000
0.111	0.001	0.000	0.004	0.000
0.167	0.001	0.000	0.004	0.000

0.222	0.002	0.000	0.005	0.000
0.278	0.002	0.000	0.006	0.000
0.333	0.002	0.000	0.006	0.000
0.389	0.002	0.001	0.007	0.000
0.444	0.002	0.001	0.007	0.000
0.500	0.002	0.001	0.008	0.000
0.556	0.002	0.001	0.008	0.000
0.611	0.003	0.001	0.008	0.000
0.667	0.003	0.001	0.009	0.000
0.722	0.003	0.001	0.009	0.000
0.778	0.003	0.002	0.010	0.000
0.833	0.003	0.002	0.010	0.000
0.889	0.004	0.002	0.010	0.000
0.944	0.004	0.002	0.011	0.000
1.000	0.004	0.002	0.011	0.000
1.056	0.004	0.003	0.011	0.000
1.111	0.004	0.003	0.011	0.000
1.167	0.005	0.003	0.012	0.000
1.222	0.005	0.003	0.012	0.000
1.278	0.005	0.004	0.012	0.000
1.333	0.005	0.004	0.013	0.000
1.389	0.006	0.004	0.013	0.000
1.444	0.006	0.004	0.013	0.000
1.500	0.006	0.005	0.013	0.000
1.556	0.006	0.005	0.014	0.000
1.611	0.007	0.006	0.014	0.000
1.667	0.007	0.006	0.014	0.000
1.722	0.007	0.006	0.014	0.000
1.778	0.007	0.007	0.014	0.000
1.833	0.008	0.007	0.015	0.000
1.889	0.008	0.008	0.015	0.000
1.944 2.000 2.056 2.111 2.167	0.008 0.009 0.009 0.009 0.009	0.008 0.008 0.009 0.009 0.010	0.015 0.015 0.016 0.016	0.000 0.000 0.000
2.222 2.278 2.333 2.389	0.010 0.010 0.010 0.011	0.010 0.011 0.012 0.012	0.016 0.016 0.016 0.017 0.017	0.000 0.000 0.000 0.000
2.444	0.011	0.013	0.017	0.000
2.500	0.011	0.013	0.017	0.000
2.556	0.012	0.014	0.018	0.000
2.611	0.012	0.015	0.019	0.000
2.667	0.013	0.015	0.020	0.000
2.722	0.013	0.016	0.021	0.000
2.778	0.013	0.017	0.023	0.000
2.833	0.014	0.018	0.024	0.000
2.889	0.014	0.018	0.026	0.000
2.944	0.014	0.019	0.028	0.000
3.000	0.015	0.020	0.030	0.000
3.056	0.015	0.021	0.032	0.000
3.111	0.016	0.022	0.034	0.000
3.167	0.016	0.023	0.036	0.000
3.222	0.016	0.023	0.038	0.000
3.278	0.017	0.024	0.040	0.000
3.333 3.389 3.444 3.500	0.017 0.018 0.018 0.019	0.025 0.026 0.027 0.028	0.042 0.045 0.047 0.049	0.000 0.000 0.000
3.556 3.611 3.667 3.722 3.778	0.019 0.019 0.020 0.020 0.021	0.029 0.030 0.031 0.033	0.051 0.054 0.057 0.060	0.000 0.000 0.000 0.000
3.833 3.889 3.944 4.000	0.021 0.021 0.022 0.022 0.023	0.034 0.035 0.036 0.037 0.039	0.062 0.065 0.068 0.071 0.074	0.000 0.000 0.000 0.000
4.056 4.111 4.167	0.023 0.023 0.024 0.024	0.040 0.041 0.042	0.266 0.616 1.069	0.000 0.000 0.000 0.000

4.444 0.027 4.500 0.027 4.556 0.028 4.611 0.028 4.667 0.029 4.722 0.029 4.778 0.030 4.833 0.031 4.889 0.031 4.944 0.032	0.047 0.048 0.049 0.051 0.053 0.054 0.056 0.057 0.059 0.061 0.062	8.028 9.043 10.10 11.19 12.32 13.49	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
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Return Period	Periods for Predeveloped Flow(cfs)
2 year	0.033515
5 year	0.056175
10 year	0.076127
25 year	0.108107
50 year	0.137638
100 year	0.172783

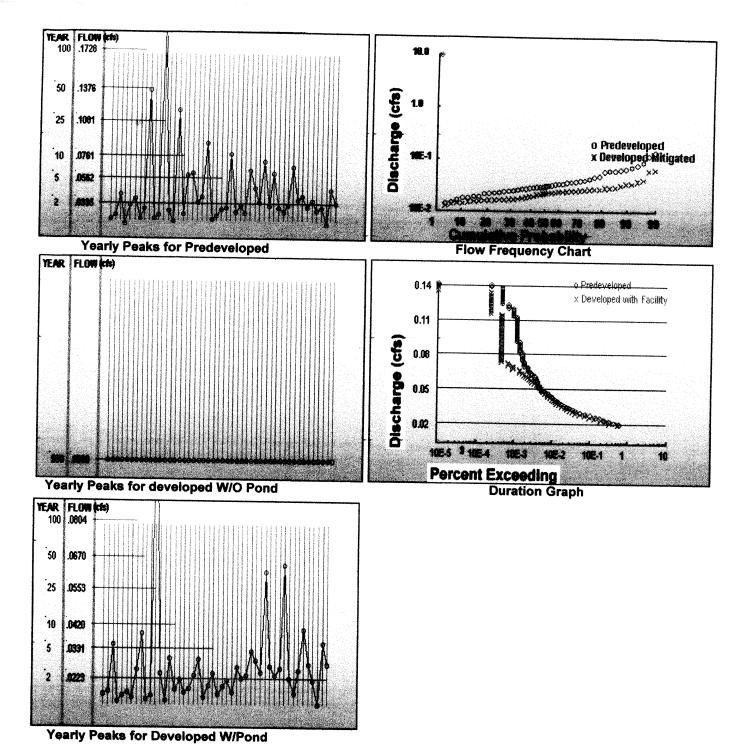
Flow Frequency Return Period	Return	Periods for Flow(cfs)	Developed	Mitigated
2 year		0.022313		
5 year		0.033123		
10 year		0.041972		
25 year		0.055333		
50 year		0.067041		
100 year		0.080409		

Yearly Peaks	for Predevelope	d and Developed-Mitigated
rear	Predeveloped	Developed
1949	0.018	0.016
1950	0.022	0.017
1951	0.042	0.035
1952	0.014	0.014
1953	0.032	0.016
1954	0.038	0.017
1955	0.019	0.015
1956	0.029	0.025
1957	0.136	0.039
1958	0.019	0.014
1959	0.023	0.016
1960	0.200	0.132
1961	0.026	0.024
1962	0.017	0.014
1963	0.118	0.030
1964	0.023	0.018
1965	0.059	0.022
1966	0.061	0.017
1967	0.034	0.018
1968	0.039	0.023
1969	0.088	0.029
1970	0.018	0.015
1971	0.022	0.020
1972	0.027	σ. 024
1973	0.029	0.016
1974	0.079	0.019
1975	0.025	0.022
1976	0.031	0.017
1977	0.024	0.026

1979 1980 1981 1982 1983 1984 1985 1986 1987 1988 1989 1990 1991 1992	0.048 0.034 0.072 0.031 0.061 0.029 0.025 0.031 0.066 0.037 0.040 0.030 0.036 0.027 0.029	0.023 0.032 0.029 0.025 0.062 0.027 0.023 0.026 0.064 0.022 0.017 0.025 0.040 0.027
1992	0.027	
1993 1994 1995 1996	0.029 0.015 0.045 0.034	0.022 0.013 0.035 0.027

	0.034	0.027	
Ranked Rank	Yearly Peaks for Predeveloped	Predeveloped and	Developed-Mitigated
1	0.1360	Developed	
2	0.1179	0.0642	
3	0.0877	0.0615	
4	0.0785	0.0403	
5	0.0716	0.0386 0.0350	
6	0.0663		
7	0.0630	0.0346	
8	0.0609	0.0322	
9	0.0607	0.0296	
10	0.0590	0.0291	
11	0.0475	0.0289	
12	0.0455	0.0274	
13	0.0419	0.0272	
14	0.0402	0.0266	
15	0.0391	0.0261	
16	0.0377	0.0257	
17		0.0254	
18	0.0368 0.0360	0.0251	
19	0.0341	0.0246	
20		0.0241	
21	0.0340	0.0240	
22	0.0337	0.0234	
23	0.0315	0.0234	
24	0.0314	0.0232	
25	0.0310	0.0222	
26 26	0.0308	0.0221	
27	0.0299	0.0220	
2.7 2.8	0.0293	0.0216	
29	0.0292	0.0216	
30	0.0290	0.0196	
30 31	0.0285	0.0193	
	0.0274	0.0185	
32	0.0270	0.0180	
33	0.0264	0.0173	
34	0.0254	0.0171	
35	0.0247	0.0170	
36	0.0238	0.0169	
37	0.0234	0.0168	
18.	0.0226	0.0164	
19	0.0225	0.0163	
0	0.0217	0.0160	
1	0.0193	0.0158	
2	0.0192	0.0153	
3	0.0183	0.0151	
4	0.0181	0.0144	
5	0.0166	0.0141	
6	0.0147	0.0138	
7	0.0141	0.0126	

Product Product Product Parcentage Pass/Fail					
0.0180 1861 1457 78.0 Pass 0.0192 1359 1125 82.0 Pass 0.0204 1031 847 82.0 Pass 0.0216 781 563 72.0 Pass 0.02253 324 237 73.0 Pass 0.0265 235 176 74.0 Pass 0.0277 179 152 84.0 Pass 0.0290 153 130 84.0 Pass 0.0314 105 97 92.0 Pass 0.0314 105 97 92.0 Pass 0.0326 90 78 86.0 Pass 0.0337 75 85.0 Pass 0.0337 53 50 94.0 Pass 0.0337 48 45 93.0 Pass 0.0377 48 45 93.0 Pass 0.0377 48 45 93.0 Pass			Final	Percentage	Pass/Fail
0.0192 1359 1125 82.0 Pass 0.0204 1031 847 82.0 Pass 0.0216 781 563 72.0 Pass 0.0229 589 422 71.0 Pass 0.0253 324 237 73.0 Pass 0.0257 179 152 84.0 Pass 0.0277 179 152 84.0 Pass 0.0290 153 130 84.0 Pass 0.0314 105 97 92.0 Pass 0.0314 105 97 92.0 Pass 0.0326 90 78 86.0 Pass 0.0339 76 66 86.0 Pass 0.0351 67 57 85.0 Pass 0.0375 53 50 94.0 Pass 0.0387 48 45 93.0 Pass 0.0412 39 34 87.0 Pass					Pass
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0.0925 5 2 40.0 Pass 0.0937 5 2 40.0 Pass 0.0949 5 2 40.0 Pass 0.0961 5 2 40.0 Pass 0.0973 5 2 40.0 Pass 0.0986 5 2 40.0 Pass 0.0998 5 2 40.0 Pass			2		
0.0937 5 2 40.0 Pass 0.0949 5 2 40.0 Pass 0.0961 5 2 40.0 Pass 0.0973 5 2 40.0 Pass 0.0986 5 2 40.0 Pass 0.0998 5 2 40.0 Pass			2		
0.0961 5 2 40.0 Pass 0.0973 5 2 40.0 Pass 0.0986 5 2 40.0 Pass 0.0998 5 2 40.0 Pass			2		
0.0961 5 2 40.0 Pass 0.0973 5 2 40.0 Pass 0.0986 5 2 40.0 Pass 0.0998 5 2 40.0 Pass		5	2		
0.0973 5 2 40.0 Pass 0.0986 5 2 40.0 Pass 0.0998 5 2 40.0 Pass					
0.0986 5 2 40.0 Pass 0.0998 5 2 40.0 Pass					
0.0998 5 2 40.0 Pass	0.0986	5	2	40.0	7
0.1010 5 2 40.0 Pass			2		7
0 1000 -	0.1010	5	2	40.0	Pass -



Project Name: pasture

Site Address:

City :

Report Date : 6/10/2004 Gage : McMillian

Data Start : 1948 **Data End** : 1996 Precip Scale: 1.00

Pan Evap Factor entered by user: 0

PREDEVELOPED LAND USE

: Basin 1

Flows To : Point of Compliance

GroundWater: No

Land Use

TILL FOREST:

Acres

DEVELOPED LAND USE

Basin : Basin 1 Flows To : Pond 1

GroundWater: No

Land Use

TILL PASTURE:

RCHRES (POND) INFORMATION

Pond Name: Pond 1
Pond Type: Trapezoidal Pond

Pond Flows to : Point of Compliance Pond Rain / Evap is not activated.

Dimensions

Depth: 5ft. Bottom Length: 2.4ft. Bottom Width : 1ft. Side slope 1: 3 To 1 Side slope 2: 3 To 1 Side slope 3: 3 To 1 Side slope 4: 3 To 1

Volume at Riser Head: 0.022 acre-ft. 958 cf

Discharge Structure

95.8 cf/2500 SF

Riser Height: 4 ft. 3.55 cy Riser Diameter: 18 in.

NotchType : Rectangular Notch Width: 0.011 ft. Notch Height: 1.726 ft.

Orifice 1 Diameter: 0.633 in. Elevation: 0 ft.

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrq(cfs)	Infilt(cfs)
0.000	0.000	0.000	0.000	0.000
0.056	0.000	0.000	0.002	
0.111	0.000	0.000		0.000
0.167	0.000		0.004	σ.000
0.107	0.000	0.000	0.004	0.000

0.222 0.000 0.278 0.000	0.000	0.005	0.000 0.000
0.333 0.000	0.000	0.006	0.000
0.389 0.000	0.000	0.007	0.000
0.444 0.000	0.000	0.007	0.000
0.500 0.000	0.000	0.007	
0.556 0.001	0.000	0.008	0.000
0.611 0.001	0.000	0.008	
0.667 0.001	0.000	0.009	0.000
0.722 0.001	0.000	0.009	
0.778 0.001	0.000	0.009	0.000
0.833 0.001	0.000	0.010	
0.889 0.001	0.000	0.010	0.000
0.944 0.001	0.000	0.010	
1.000 0.001 1.056 0.001	0.001	0.011 0.011	0.000
1.111 0.002	0.001	0.011	0.000
1.167 0.002	0.001	0.011	
1.222 0.002	0.001	0.012	0.000
1.278 0.002	0.001	0.012	
1.333 0.002	0.001	0.012	0.000
1.389 0.002	0.001	0.012	
1.444 0.002	0.001	0.013	0.000
1.500 0.003	0.002	0.013	
1.556 0.003	0.002	0.013	0.000
1.611 0.003	0.002	0.013	
1.667 0.003 1.722 0.003	0.002 0.002	0.014	0.000
1.778 0.003 1.833 0.004	0.002 0.003	0.014	0.000
1.889 0.004	0.003	0.014	0.000
1.944 0.004	0.003	0.015	
2.000 0.004 2.056 0.005	0.003	0.015 0.015	0.000
2.111 0.005 2.167 0.005	0.004	0.015 0.015	0.000
2.222 0.005	0.004	0.016	0.000
2.278 0.005	0.005	0.016	0.000
2.333 0.006	0.005	0.017	0.000
2.389 0.006	0.005	0.018	
2.444 0.006	0.006	0.019	0.000
2.500 0.006	0.006	0.020	
2.556 0.007 2.611 0.007	0.006 0.007	0.022	0.000
2.667 0.007	0.007	0.025	0.000
2.722 0.007	0.007	0.027	
2.778 0.008 2.833 0.008	0.008	0.029 0.031	0.000
2.889 0.008 2.944 0.009	0.009	0.033	0.000
3.000 0.009 3.056 0.009	0.010	0.038	0.000
3.111 0.010 3.167 0.010	0.011	0.042	0.000
3.222 0.010 3.278 0.010	0.012 0.012	0.046	0.000
3.333 0.011	0.013	0.051	0.000
3.389 0.011	0.014	0.054	
3.444 0.011 3.500 0.012	0.014	0.057	0.000
3.556 0.012	0.016	0.062	0.000
3.611 0.013	0.016	0.065	
3.667 0.013	0.017	0.068	0.000
3.722 0.013	0.018	0.071	
3.778 0.014	0.018	0.075	0.000
3.833 0.014	0.019	0.078	
3.889 0.014 3.944 0.015	0.020	0.081	0.000
4.000 0.015	0.022	0.088	0.000
4.056 0.016	0.022	0.279	
4.111 0.016	0.023	0.629	0.000
4.167 0.016	0.024	1.082	

5.000 0.023 0.041 14.70 0.000	4.222 4.278 4.333 4.389 4.444 4.500 4.556 4.611 4.667 4.722 4.778 4.833 4.889 4.944 5.000	0.017 0.017 0.018 0.018 0.019 0.019 0.020 0.020 0.021 0.021 0.022 0.022 0.023 0.023	0.025 0.026 0.027 0.028 0.029 0.030 0.031 0.032 0.033 0.034 0.036 0.037 0.038 0.039 0.041	1.618 2.227 2.900 3.631 4.417 5.254 6.138 7.068 8.041 9.056 10.11 11.20 12.33 13.50 14.70	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
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Flow Frequency Return Return Period	n Periods for Predeveloped Flow(cfs)
2 year	0.033515
5 year	0.056175
10 year	0.076127
25 year	0.108107
50 year	0.137638
100 year	0.172783

Flow Frequency	Return	Periods for	Developed Mitigated
Return Period		Flow(cfs)	
2 year		0.023418	
5 year		0.034491	
10 year		0.043502	
25 year		0.057035	
50 year		0.068841	
100 year		0-082271	

Yearly	Peaks	for Predevelo	ped and Developed-Mitigated
Year		Predeveloped	Developed
1949		0.018	0.015
1950		0.022	0.019
1951		0.042	0.032
1952		0.014	0.013
1953		0.032	0.016
1954		0.038	0.018
1955		0.019	0.015
1956		0.029	0.027
1957		0.136	0.049
1958		0.019	0.014
1959		0.023	0-017
1960		0.200	0.142
1961		0.026	0.025
1962		0.017	0.013
1963		0.118	0.043
1964		0.023	0.021
1965		0,059	0.023
1966		0.061	0.021
1967		0.034	0.021
1968		0.039	0.025
1969		0.088	0.034
1970		0.018	0.016
1971		0.022	0.021
1972		0.027	0.026
1973		0.029	0.016
1974		0.079	0.028
1975		0.025	0.024
1976		0.031	0.019
1977		0.024	0,025

1979	0.048	0-025
1980	0.034	0.033
1981	0.072	0.033
1982	0.031	0.025
1983	0.061	0.047
1984	0.029	0.028
1985	0.025	0.023
1986	0.031	0.028
1987	0.066	0.054
1988	0.037	0.023
1989	0.040	0.019
1990	0.030	0.028
1991	0.036	0.030
1992	0.027	0.027
1993	0.029	0.025
1994	0.015	0.013
1995	0.045	0.033
1996	0.034	0.027

Predeveloped

0.0340

0.0337

0.0315

0.0314

0.0310

0.0308

0.0299

0.0293

0.0292

0.0290

0.0285

0.0274

0.0270

0.0264

0.0254

0.0247

Rank

20

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	•	·
1	0.1360	0.0536
2	0.1179	0.0494
3	0.0877	0.0474
4	0.0785	0.0428
5	0.0716	0.0343
6	0.0663	0.0334
7	0.0630	0.0334
8	0.0609	0.0328
9	0.0607	0.0321
10	0.0590	0.0296
11	0.0475	0.0284
12	0.0455	0.0278
13	0.0419	0.0277
14	0.0402	0.0276
15	0.0391	0.0274
1.6	0.0377	0.0271
17	0.0368	0.0267
18	0.0360	0.0258
19	0.0341	0.0252

0.0251

0.0251

0.0249

0.0248

0.0247

0.0245

0.0242

0.0233

0.0232

0.0229

0.0215

0.0213

0.0211

0.0208

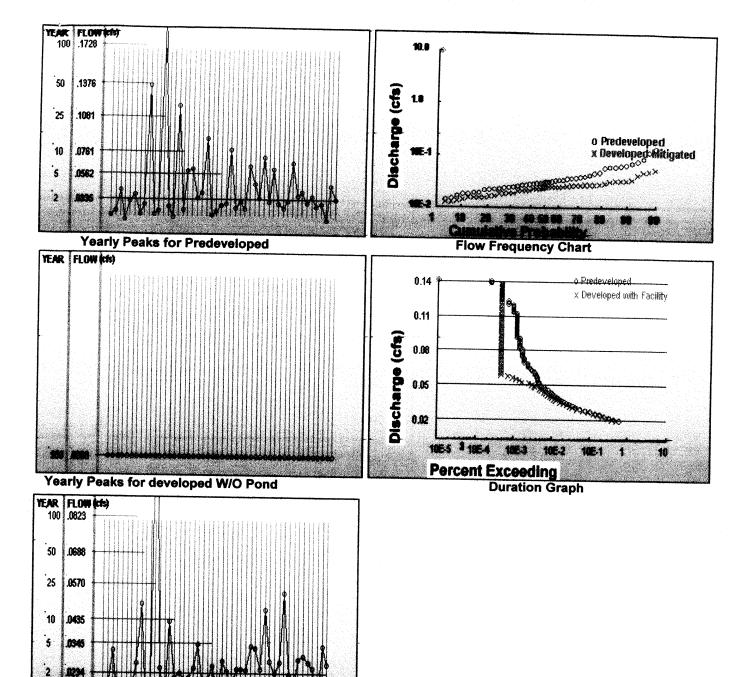
0.0188

0.0187

Ranked Yearly Peaks for Predeveloped and Developed-Mitigated

Developed

Flow (CFS) Predev	Final	Percentage	Page/Egil
0.0168	2564	2158	84.0	Pass
0.0180	1861	1687	90.0	Pass
0.0192	1359	1252	92.0	Pass
0.0204	1031	936	90.0	Pass
0.0216	781	714	91.0	Pass
0.0229 0.0241	589	535	90.0	Pass
0.0253	440 324	390 286	88.0 88.0	Pass
0.0265	235	199	84.0	Pass Pass
0.0277	179	152	84.0	Pass
0.0290	153	128	83.0	Pass
0.0302	124	109	87.0	Pass
0.0314	105	90	85.0	Pass
0.0326	90	70	77.0	Pass
0.0339 0.0351	76 67	56 50	73.0	Pass
0.0363	59	50 44	74.0 74.0	Pass
0.0375	53	39	73.0	Pass Pass
0.0387	48	34	70.0	Pass
0.0400	43	30	69.0	Pass
0.0412	39	27	69.0	Pass
0.0424	35	23	65.0	Pass
0.0436 0.0448	29 27	21	72.0	Pass
0.0461	23	16 15	59.0 65.0	Pass
0.0473	22	13	59.0	Pass Pass
0.0485	20	11	55.0	Pass
0.0497	19	7	36.0	Pass
0.0509	18	6	33.0	Pass
0.0522	18	5	27.0	Pass
0.0534 0.0546	18 17	4	22.0	Pass
0.0558	16	3 2	17.0 12.0	Pass
0.0571	16	2	12.0	Pass Pass
0.0583	15	2	13.0	Pass
0.0595	13	2	15.0	Pass
0.0607	12	2	16.0	Pass
0.0619	11	2	18.0	Pass
0.0632 0.0644	10	2 2	20.0	Pass
0.0656	10 10		20.0	Pass
0.0668	8	2	25.0	Pass
0.0680	8	2 2 2 2	25.0	Pass Pass
0.0693	8	2	25.0	Pass
0.0705	8	2 2 2 2 2 2 2 2 2	25.0	Pass
0.0717	7	2	28.0	Pass
0.0729 0.0741	7 7	2	28.0	Pass
0.0754	7	2	28.0 28.0	Pass
0.0766	7	2	28.0	Pass Pass
0.0778	7	2	28.0	Pass
0.0790	6	2	33.0	Pass
0.0803	6	2 2	33.0	Pass
0.0815	6	2	33.0	Pass
0.0827 0.0839	6 6	2 2	33.0 33.0	Pass
0.0851	6	2	33.0	Pass Pass
0.0864	6	2 2 2 2 2	33.0	Pass
0.0876	6	2	33.0	Pass
0.0888	5	2	40.0	Pass
0.0900	5	2	40.0	Pass
0.0912 0.0925	5 5	2 2 2	40.0	Pass
0.0925	5	2	40.0	Pass
0.0949	5	2	40.0	Pass Pass
0.0961	5	2	40.0	Pass
0.0973	5	2	40.0	Pass
0.0986	5	2	40.0	Pass
0.0998	5	2	40.0	Pass
0.1010 0.1022	5 5	2 2 2 2 2 2 2 2	40.0	Pass
0.1022	J	2	40.0	Pass



Yearly Peaks for Developed W/Pond

APPENDIX F

WWHM Output for Green Roof vs. Standard Roof

WESTERN WASHINGTON HYDROLOGY MODEL V2 PROJECT REPORT

Project Name: Roof(imp)

Site Address:

City :

Report Date : 6/9/2004
Gage : McMillian

Data Start : 1948 Data End : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

Basin

: Pre-Dev

Flows To : Point of Compliance

GroundWater: No

Land Use

TILL FOREST:

0.23

DEVELOPED LAND USE

Basin : Dev Flows To : Pond 1

GroundWater: No

Land Use

Acres

IMPERVIOUS:

0.23

RCHRES (POND) INFORMATION

Pond Name: Pond 1
Pond Type: Trapezoidal Pond Pond Flows to : Point of Compliance Pond Rain / Evap is not activated.

Dimensions

Depth: 5ft. Bottom Length: 37.84ft. Bottom Width: 12.56ft. Side slope 1: 3 To 1 Side slope 2: 3 To 1
Side slope 3: 3 To 1
Side slope 4: 3 To 1

Volume at Riser Head: 0.117 acre-ft. 5097 cf → 188.78 cf

Discharge Structure Riser Height: 4 ft. Riser Diameter: 18 in. NotchType : Rectangular Notch Width: 0.010 ft. Notch Height: 0.464 ft.

Orifice 1 Diameter: 0.23533 in. Elevation: 0 ft.

Pond Hydraulic Table

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt(cfs)
0.000	0.011	0.000	0.000	0.000
0.056	0.011	0.001	0.000	0.000
0.111	0.012	0.001	0.000	0.000
0.167	0.012	0.002	0.001	0.000
0.222	0.012	0.003	0.001	0.000

0.278	0.013	0.003	0.001	0.000
0.333	0.013	0.004	0.001	0.000
0.389	0.014	0.005	0.001	0.000
0.444	0.014	0.006	0.001	0.000
0.500	0.015	0.006	0.001	0.000
0.556	0.015	0.007	0.001	0.000
0.611	0.015	0.008	0.001	0.000
0.667	0.016	0.009	0.001	0.000
0.722	0.016	0.010	0.001	
0.778	0.017	0.011	0.001	0.000
0.833	0.017	0.012	0.001	0.000
0.889	0.018	0.013	0.001	0.000
0.944	0.018	0.014	0.001	0.000
1.000	0.019	0.015	0.001	0.000
1.056	0.019	0.016	0.001	0.000
1.111 1.167 1.222	0.020 0.020 0.021	0.017 0.018	0.002 0.002	0.000 0.000
1.278 1.333	0.021 0.022	0.019 0.020 0.021	0.002 0.002 0.002	0.000 0.000 0.000
1.389	0.022	0.023	0.002	0.000
1.444	0.023	0.024	0.002	0.000
1.500	0.023	0.025	0.002	0.000
1.556	0.024	0.026	0.002	0.000
1.611	0.024	0.028	0.002	0.000
1.667	0.025	0.029	0.002	0.000
1.722	0.025	0.030	0.002	0.000
1.778	0.026	0.032	0.002	
1.833	0.026	0.033	0.002	0.000
1.889	0.027	0.035	0.002	0.000
1.944	0.028	0.036	0.002	0.000
2.000	0.028	0.038	0.002	0.000
2.056	0.029	0.039	0.002	0.000
2.111	0.029	0.041	0.002	0.000
2.167	0.030	0.043	0.002	0.000
2.222	0.030	0.044	0.002	0.000
2.278	0.031	0.046	0.002	0.000
2.333	0.032	0.048	0.002	0.000
2.389	0.032	0.050	0.002	0.000
2.444	0.033	0.051	0.002	0.000
2.500	0.033	0.053	0.002	0.000
2.556	0.034	0.055	0.002	0.000
2.611	0.035	0.057	0.002	0.000
2.667	0.035	0.059	0.002	0.000
2.722	0.036	0.061	0.002	0.000
2.778	0.037	0.063	0.002	0.000
2.833	0.037	0.065	0.002	
2.889	0.038	0.067	0.002	0.000
2.944	0.039	0.069	0.002	0.000
3.000	0.039	0.071	0.003	0.000
3.056	0.040	0.074	0.003	0.000
3.111	0.041	0.076	0.003	0.000
3.167	0.041	0.078	0.003	0.000
3.222	0.042	0.080	0.003	0.000
3.278	0.043	0.083	0.003	0.000
3.333	0.043	0.085	0.003	0.000
3.389	0.044	0.088	0.003	0.000
3.444	0.045	0.090	0.003	
3.500	0.045	0.093	0.003	0.000
3.556	0.046	0.095	0.003	0.000
3.611	0.047	0.098	0.003	0.000
3.667	0.047	0.100	0.004	0.000
3.722	0.048	0.103	0.005	0.000
3.778	0.049	0.106	0.007	0.000
3.833	0.050	0.108	0.008	0.000
3.889	0.050	0.111	0.010	0.000
3.944	0.051	0.114	0.011	0.000
4.000	0.052	0.117	0.013	0.000
4.056	0.053	0.120	0.204	
4.111	0.053	0.123	0.554	0.000
4.167	0.054	0.126	1.007	0.000
4.222	0.055	0.129	1.543	0.000

4.278	0.056	0.132	2.152	0.000
4.333	0.057	0.135	2.824	0.000
4.389	0.057	0.138	3.556	0.000
4.444	0.058	0.141	4.341	0.000
4.500	0.059	0.144	5.178	0.000
4.556	0.060	0.148	6.062	0.000
4.611	0.060	0.151	6.992	0.000
4.667	0.061	0.155	7.965	0.000
4.722	0.062	0.158	8.979	0.000
4.778	0.063	0.161	10.03	0.000
4.833	0.064	0.165	11.13	0.000
4.889	0.065	0.168	12.26	0.000
4.944	0.065	0.172	13.42	0.000
5.000	0.066	0.176	14.62	0.000

ANALYSIS RESULTS

Flow Frequency Return	Periods for Predeveloped
Return Period	Flow(cfs)
2 year	0.005062
5 year	0.008492
10 year	0.011064
25 year	0.014607
50 year	0.017437
100 year	0.020415

Flow Frequency Return Period	Return Periods for Flow(cfs)	Developed Mitigated
2 year	0.002807	
5 year	0.00435	
10 year	0.005657	
25 year	0.007686	
50 year	0.009509	
100 year	0.011634	

Yearly	Peaks	for Predevelop	oed and Developed-Mitigate
Year		Predeveloped	Developed
1949		0.007	0.003
1950		0.006	0.003
1951		0.012	0.010
1952		0.003	0.002
1953		0.004	0.007
1954		0.004	0.002
1955		0.004	0.002
1956		0.008	0.007
1957		0.003	0.002
1958		0.003	0.002
1959		0.004	0.003
1960		0.022	0.003
1961		0.006	0.012
1962		0.002	0.002
1963		0.015	0.003
1964		0.006	0.003
1965		0.005	0.003
1966		0.014	0_002
1967		0.007	0.002
1968		0.003	0.002
1969		0.004	0.002
1970		0.003	0.003
1971		0.005	0.003
1972		0.008	0.005
1973		0.003	0.003
1974		0.010	0.002
1975		0.006	0.003
1976		0.006	0.003
1977		0.001	0.002
1977		0.012	0.002

1980	0.008	0.005
1981	0.004	0.003
1982	0.007	0.005
1983	0.004	0.002
1984	0.002	0.002
1985	0.003	0.003
1986	0.005	0.002
1987	0.013	0.014
1988	0.004	0.002
1989	0.003	0.003
1990	0.007	0.007
1991	0.006	0.002
1992	0.004	0.002
1993	0.007	0.002
1994	0.002	0.002
1995	0.002	0.002
1996	0.007	0.003

		0,003
Ranked	Yearly Peaks for	Predeveloped and Developed-Mitigated
Rank	Predeveloped	Developed
1 2	0.0147	0.0122
3	0.0139	0.0104
4	0.0130	0.0074
5	0.0122	0.0068
6	0.0116	0.0068
7	0.0098	0.0051
8	0.0083	0.0048
9	0.0079	0.0047
10	0.0078	0.0027
	0.0073	0.0027
11	0.0069	0.0026
12	0.0069	0.0026
13	0.0069	0.0026
14	0.0068	0.0026
15	0.0066	0.0026
16	0.0064	0.0026
17	0.0062	0.0025
18 19	0.0062	0.0025
	0.0061	0.0025
20	0.0060	0.0025
21 22	0.0058	0.0025
23	0.0056	0.0025
	0.0055	0.0025
24	0.0055	0.0025
25	0.0047	0.0025
26	0.0044	0.0025
27 28	0.0044	0.0025
20 29	0.0044	0.0025
30	0.0042	0.0025
31	0.0040	0.0025
32	0.0039	0-0024
33	0.0037	0.0024
34	0.0037	0.0024
35	0.0035 0.0034	0.0024
36	0.0034	0.0023
37	0.0033	0.0023
38	0.0033	0.0023
39	0.0031	0.0023
40	0.0030	0.0022
41	0.0030	0.0022 0.0022
42	0.0026	0.0022
43	0.0020	0.0022
44	0.0019	0.0021
45	0.0019	0.0021
46	0.0017	0.0021
47	0.0009	0.0019
	J. 0005	0,001)

0.0077 0.0078 0.0080 0.0081 0.0083 0.0084 0.0086 0.0087 0.0089 0.0099 0.0092 0.0093 0.0095 0.0098 0.0099 0.0101 0.0102 0.0104 0.0105 0.0107 0.0108 0.0110 0.0111 0.0113 0.0114 0.0116 0.0117 0.0119 0.0120 0.0122 0.0123 0.0125 0.0126 0.0128 0.0129	4173 3163 3165 2222 1980 113173 1105 113173 1105 1105 1105 1105 1105 1105 1105 110	3925 77193 66194 77193 66194 77193 66194 77193 7	94.0 45.0 25.0 26.0 28.0 29.0 30.0 31.0 31.0 31.0 31.0 31.0 31.0 31.0 31.0 32.0 33.0 34.0 37.0 38.0 39.0 41.0 44.0 45.0 44.0 45.0 44.0 45.0 44.0 45.0 44.0 45.0 44.0 45.0 47.0 49.0 50.0 55.0 58.0 63.0 66.0 70.0 70.0 71.0 76.0 70.0	Passssssssssssssssssssssssssssssssssss
	3	2	66.0	Pass Pass

0.0134 0.0135 0.0137 0.0138 0.0140 0.0141 0.0143 0.0144 0.0146 0.0147 0.0149 0.0150 0.0152 0.0155 0.0155 0.0156 0.0158 0.0159 0.0161 0.0162 0.0164 0.0165 0.0165 0.0165 0.0167 0.0168 0.0170 0.0171 0.0173 0.0174	3 3 3 3 2 2 2 2 2 1 1 1 1 1 1 1 1 1 1 1	2 2 2 2 2 2 1 0 0 0 0 0 0 0 0 0 0 0 0 0	66.0 66.0 66.0 100.0 100.0 50.0 .0 .0 .0 .0	Passs Pass Pass Passs Pas
--	--	--	--	---

Water Quality BMP Flow and Volume.

On-line facility volume: 4-004-acre-feet 0.025

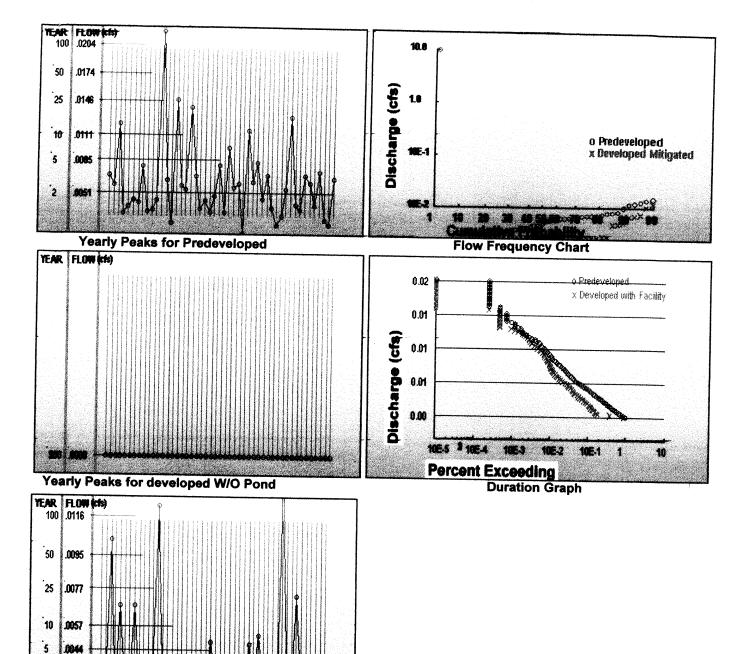
On-line facility target flow: 0 cfs.

Adjusted for 15 min: 0 cfs.

Off-line facility target flow: 0 cfs.

Adjusted for 15 min: 0 cfs.

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Yearly Peaks for Developed W/Pond

WESTERN WASHINGTON HYDROLOGY MODEL V2 PROJECT REPORT

Project Name: Green Roof

Site Address:

City :

Report Date : 6/9/2004 Gage : McMillian

Data Start : 1948 **Data End** : 1996 Precip Scale: 1.00

PREDEVELOPED LAND USE

: Pre-Dev

Flows To : Point of Compliance

GroundWater: No

Land Use

TILL FOREST:

0.23

DEVELOPED LAND USE

Basin : Dev Flows To : Pond 1 GroundWater: No

Land Use

Acres

TILL GRASS:

0.23

RCHRES (POND) INFORMATION

Pond Name: Pond 1
Pond Type: Trapezoidal Pond

Pond Flows to : Point of Compliance Pond Rain / Evap is not activated.

Dimensions

Depth: 5ft. Bottom Length: 9.9ft. Bottom Width: 3.2ft. Side slope 1: 3 To 1 Side slope 2: 3 To 1 Side slope 3: 3 To 1 Side slope 4: 3 To 1

Volume at Riser Head: 0.035 acre-ft. 1525 CF -> 56.48 Cf

Discharge Structure Riser Height: 4 ft. Riser Diameter: 18 in. NotchType : Rectangular Notch Width: 0.010 ft. Notch Height: 0.440 ft.

Orifice 1 Diameter: 0.232 in. Elevation: 0 ft.

Pond Hydraulic Table

Stage (ft)	Area (acr)	Volume (acr-ft)	Dschrg(cfs)	Infilt(cfs)
0.000	0.001	0.000	0.000	0.000
0.056	0.001	0.000	0.000	0.000
0.111	0.001	0.000	0.000	0.000
0.167	0.001	0.000	0.001	0.000
0.222	0.001	0.000	0.001	0.000

0.278	0.001	0.000	0.001	0.000	
0.333 0.389	0.001	0.000	0.001	0.000	
0.444 0.500	0.002 0.002	0.001 0.001	0.001 0.001	0.000 0.000	
0.556 0.611	0.002 0.002	0.001 0.001	0.001 0.001	0.000	
0.667 0.722	0.002 0.002	0.001 0.001	0.001	0.000	
0.778 0.833	0.003 0.003	0.001	0.001 0.001	0.000	
0.889	0.003	0.002	0.001 0.001	0.000	•
1.000	0.003	0.002 0.002	0.001	0.000	
1.111 1.167	0.004	0.002 0.003	0.001 0.001 0.002	0.000 0.000 0.000	
1.222	0.004	0.003	0.002 0.002	0.000	
1.333	0.005 0.005	0.003	0.002 0.002 0.002	0.000	
1.444	0.005	0.004	0.002 0.002	0.000	
1.556 1.611	0.006	0.004	0.002 0.002	0.000	
1.667 1.722	0.006	0.005 0.005	0.002	0.000	
1.778 1.833	0.007 0.007	0.006	0.002 0.002	0.000	
1.889 1.944	0.007 0.007	0.006 0.007	0.002	0.000	
2.000 2.056	0.008	0.007	0.002	0.000	
2.111 2.167	0.008	0.008	0.002	0.000	
2.222 2.278	0.009 0.009	0.009 0.010	0.002	0.000	
2.333 2.389	0.009 0.010	0.010 0.011	0.002	0.000	
2.444 2.500	0.010 0.010	0.011 0.012	0.002 0.002	0.000	
2.556 2.611	0.011 0.011	0.012 0.013	0.002 0.002	0.000	
2.667 2.722	0.011	0.014 0.014	0.002	0.000 0.000	
2.778 2.833	0.012 0.012	0.015 0.016	0.002 0.002	0.000	
2.889 2.944	0.013 0.013	0.016 0.017	0.002 0.002	0.000 0.000	
3.000 3.056	0.014 0.014	0.018 0.019	0.002 0.002	0.000 0.000	
3.111 3.167	0.014 0.015	0.019 0.020	0.002 0.003	0.000 0.000	
3.222 3.278	0.015 0.016	0.021 0.022	0.003 0.003	0.000 0.000	
3.333 3.389	0.016 0.016	0.023 0.024	0.003 0.003	0.000 0.000	
3.444	0.017 0.017	0.024 0.025	0.003 0.003	0.000 0.000	
3.556 3.611	0.018 0.018	0.026 0.027	0.003 0.003	0.000 0.000	
3.667 3.722	0.018 0.019	0.028 0.029	0.004 0.005	0.000	
3.778	0.019 0.020	0.030 0.032	0.006 0.007	0.000	
3.889	0.020	0.033	0.009 0.010	0.000	
4.000 4.056	0.021 0.022	0.035 0.036	0.012 0.203	0.000	
4.111	0.022 0.023	0.037	0.553 1.006	0.000	
4.222	0.023	0.040	1.542	0.000	

4.278 4.333 4.389 4.444 4.500 4.556 4.611 4.667 4.722 4.778 4.833 4.889 4.944 5.000	0.024 0.024 0.025 0.025 0.026 0.026 0.027 0.027 0.028 0.028 0.029 0.029	0.041 0.043 0.044 0.045 0.047 0.048 0.050 0.051 0.053 0.054 0.056 0.057	2.151 2.823 3.555 4.340 5.177 6.061 6.991 7.964 8.978 10.03 11.13 12.25 13.42	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
5.000	0.030	0.059	13.42	0.000

ANALYSIS RESULTS

Flow	Frequency	Return	Periods	for	Predeveloped
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Return Period	Flow(cis)
2 year	0.005062
5 year	0.008492
10 year	0.011064
25 year	0.014607
50 year	0.017437
100 year	0.020415

Flow Frequency Return Periods for Developed Unmitigated

Return Period	Flow(cfs)
2 year	0.014612
5 year	0.025071
10 year	0.034044
25 year	0.048054
50 year	0.060658
100 year	0.075321

Flow Frequency Return Periods for Developed Mitigated

Return Period	Flow(cfs)
2 year	0.002766
5 year	0.004178
10 year	0.005348
25 year	0.007136
50 year	0.008718
100 year	0.010539

Yearly Peaks for Predeveloped and Developed-Mitigated

Year	Predeveloped	Developed
1949	0.007	0.002
1950	0.006	0.003
1951	0.012	0.010
1952	0.003	0.002
1953	0.004	0.003
1954	0.004	0.002
1955	0.004	0.002
1956	0.008	0.003
1957	0.003	0.002
1958	0.003	0.002
1959	0.004	0.002
1960	0.022	0.007
1961	0.006	0.007
1962	0.002	0.002
1963	0.015	0.003
1964	0.006	0-002
1965	0.005	0.003
1966	0.014	0.002
1967	0.007	0.002
1968	0.003	0.002
1969	0.004	0.002

1970 1971 1972 1973 1974 1975 1976 1977 1978 1979 1980 1981 1982 1983 1984 1985 1986 1987 1988 1989 1990 1991 1992	0.003 0.005 0.008 0.003 0.010 0.006 0.006 0.001 0.012 0.006 0.008 0.004 0.007 0.004 0.002 0.003 0.005 0.013 0.004 0.003 0.007 0.006	0.002 0.002 0.006 0.003 0.002 0.003 0.002 0.002 0.002 0.003 0.006 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002
1992 1993	0.004	0.003 0.002
1994 1995 1996	0.002 0.002 0.007	0.002 0.002 0.005

Ranked Yearly Peaks for Predeveloped and Developed-Mitigated Rank Predeveloped Developed

Rank	Predeveloped	Developed
1	0.0147	0.0099
2	0.0139	0.0075
3	0.0130	0.0072
4	0.0122	0.0066
5	0.0116	0.0062
6	0.0098	0.0058
7	0.0083	0.0051
8	0.0079	0.0048
9	0.0078	0.0030
10	0.0073	0.0026
11	0.0069	0.0026
12	0.0069	0.0026
13	0.0069	0.0026
14	0.0068	0-0026
15	0.0066	0.0025
16	0.0064	0.0025
17	0.0062	0.0025
18	0.0062	0.0025
19	0.0061	0.0025
20	0.0060	0.0025
21	0.0058	0.0025
22	0.0056	0.0025
23	0.0055	0.0025
24	0.0055	0.0025
25	0.0047	0.0025
26	0.0044	0.0025
27	0.0044	0.0025
28	0.0044	0.0024
29	0.0042	0.0024
30	0.0040	0.0024
31	0.0039	0.0024
32	0.0037	0.0024
33	0.0037	0.0024
34	0.0035	0.0024
35	0.0034	0.0023
36	0.0033	0_0023
37	0.0033	0.0023
38	0.0031	0.0023
39	0.0030	0.0023
40	0.0030	0.0023
41	0.0030	0.0022

42	0.0026	0.0021
43	0.0022	0.0021
44	0.0019	0.0020
45	0.0018	0.0020
46	0.0017	0.0019
47	0.0009	0.0019

1/2 2 year	r to 50	vear		
Flow (CFS)	Predev	Final	Percentage	Pass/Fail
0.0025	4173	2676	64.0	Pass
0.0027	3630	944	26.0	Pass
0.0028	3165	883	27.0	Pass
0.0030	2780	823	29.0	Pass
0.0031	2463	770	31.0	Pass
0.0033	2202	740	33.0	Pass
0.0034 0.0036	1991 1805	717 690	36.0 38.0	Pass Pass
0.0036	1620	659	40.0	Pass Pass
0.0039	1456	629	43.0	Pass
0.0040	1310	604	46.0	Pass
0.0042	1173	570	48.0	Pass
0.0043	1054	535	50.0	Pass
0.0045	937	504	53.0	Pass
0.0046	842	467	55.0	Pass
0.0048	746	427	57.0	Pass
0.0049	667	394	59.0	Pass
0.0051 0.0052	602 542	354 319	58.0 58.0	Pass
0.0054	480	289	60.0	Pass Pass
0.0055	433	264	60.0	Pass
0.0057	378	236	62.0	Pass
0.0058	332	215	64.0	Pass
0.0060	293	193	65.0	Pass
0.0061	261	176	67.0	Pass
0.0063	236	158	66.0	Pass
0.0064	209	145	69.0	Pass
0.0066	184	120	65.0	Pass
0.0067	171	112	65.0	Pass
0.0069	157	104	66.0	Pass
0.0070 0.0072	143 129	96 81	67.0 62.0	Pass
0.0072	120	75	62.0	Pass Pass
0.0075	114	66	57.0	Pass
0.0077	105	64	60.0	Pass
0.0078	95	63	66.0	Pass
0.0080	89	61	68.0	Pass
0.0081	80	59	73.0	Pass
0.0083	72	57	79.0	Pass
0.0084	65	54	83.0	Pass
0.0086	60	53	88.0	Pass
0.0087	56	51	91.0	Pass
0.0089	50	48	96-0	Pass
0.0090 0.0092	47 46	45 42	95.0 91.0	Pass Pass
0.0093	42	39	92.0	Pass
0.0095	39	37	94.0	Pass
0.0096	36	34	94.0	Pass
0.0098	34	31	91.0	Pass
0.0099	31	23	74.0	Pass
0.0101	29	22	75.0	Pass
0.0102	26	22	84.0	Pass
0.0104	24	21	87.0	Pass
0.0105	23	19	82.0	Pass
0.0107	22	18	81.0	Pass
0.0108 0.0110	18 17	17 15	94.0 88.0	Pass Pass
0.0111	14	14	100.0	Pass Pass
0.0111	12	13	108.0	Pass
0.0114	10	11	110.0	Pass
0.0116	10	10	100.0	Pass
0.0117	8	7	87.0	Pass

0.0119 0.0120 0.0122 0.0123 0.0125 0.0126 0.0128 0.0129 0.0131 0.0132 0.0134 0.0135 0.0137 0.0144 0.0143 0.0144 0.0146 0.0147 0.0149 0.0150 0.0152 0.0153 0.0155 0.0158 0.0155 0.0158 0.0159 0.0161 0.0162 0.0164 0.0165 0.0165 0.0167 0.0168 0.0170 0.0171 0.0173 0.0174	8 7 7 6 5 5 5 4 3 3 3 3 2 2 2 2 1 1 1 1 1 1 1 1 1 1 1 1	7754443222210000000000000000000000000000000	87.0 100.0 71.0 66.0 80.0 80.0 66.0 66.0 66.0 .0 .0 .0 .0 .0 .0 .0 .0	Passssssssssssssssssssssssssssssssssss
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Water Quality BMP Flow and Volume.

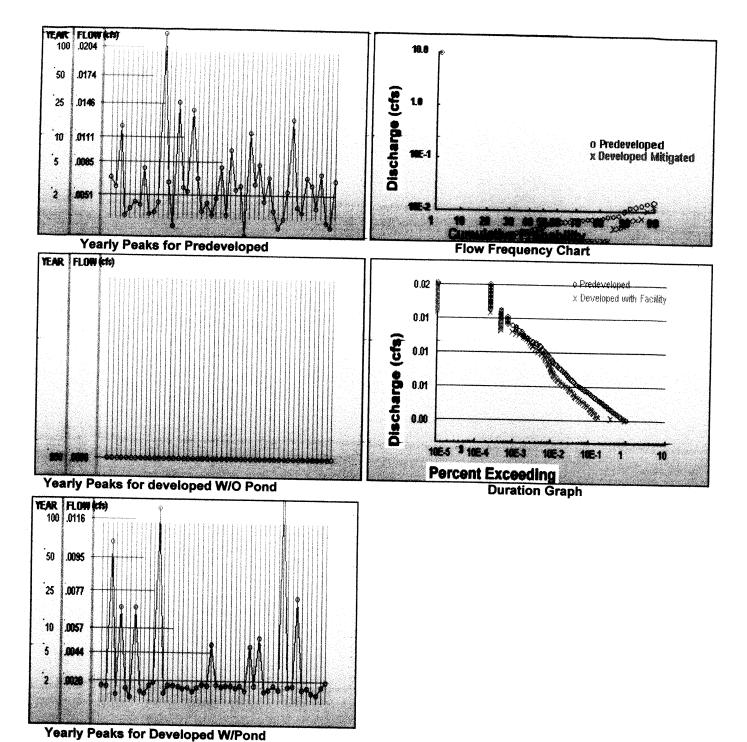
On-line facility volume: 0.01 acre-feet On-line facility target flow: 0 cfs.

Adjusted for 15 min: 0 cfs.

Off-line facility target flow: 0 cfs.

Adjusted for 15 min: 0 cfs.

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APPENDIX G

Kensington Estates Case Study by AHBL, dated February 6, 2002.

PROJECT MEMO

To:

FROM: Glenn Hume

DATE: February 6, 2002

PROJECT: Low Impact Development

OUR FILE NO.: 201462.30

SUBJECT: WWHM Comparison Analysis



The purpose of this analysis was to provide general comparisons for the total volume of stormwater storage required for a conventional residential development versus a low impact development (LID) design by utilizing the new Department of Ecology (DOE) standards. Kensington Estates, a residential development in Pierce County on a 23.92-acre site approximately 4 miles south of Puyallup, was used as the case study site. The Western Washington Hydrology Model (WWHM) developed by the DOE was utilized as the design tool in sizing conceptual stormwater facilities. The WWHM is an continuous model based on HSPF developed by DOE to provide a tool to design and analyze a storm facility's ability to meet the new DOE requirements of matching pre-developed and developed peak flows and also matching flow durations from half the 2-year storm to the 50-year design storm. This new quantity control requirement, established in the Stormwater Management Manual for Western Washington, August 2001, is similar to the King County requirements for Level 2 quantity control. Following is a list of the assumptions and input used to compare the stormwater storage requirement for conventional development versus Low impact development. The resulting volumes are provided in the attached table for comparison (see Attachment #1).

General Assumptions:

- 1. The total site area is 23.92 acres.
- 2. Soils are predominately Type C soils, modeled as till soils in the WWHM.
- 3. There is an existing wetland located near the south portion of the property line.
- 4. Existing conditions are predominately forested (pre-developed conditions of forest are required by the WWHM unless there is historical evidence that the property was pasture prior to the influence of man.)

Conventional Development Assumptions:

- 1. Area input values for conventional development analysis were obtained from the Pierce County Low Impact Development Study by CH2MHILL, dated April 11, 2001.
- 2. All roof drains are tight-lined to closed-pipe conveyance system located in the road network.

- 3. Roads consists of asphalt concrete pavement with curb and gutter and sidewalk. Stormwater conveyance is through a network of catch basins and closed pipe discharging directly to the quantity control facility.
- 4. The developed site was modeled as a single basin.
- 5. Existing wetland and wetland buffer area was not included in the basin input for predeveloped or developed basins.
- 6. The conventional design utilizes a single detention facility. The detention design was evaluated using the WWHM and the new DOE standards.
- 7. Stormwater quality requirements are met via a wetpond. The required wetpond volume was calculated utilizing the Waterworks program. Waterworks is an event-based program that utilizes the Santa Barbara Urban Hydrograph (SBUH) method with Type a 1A rainfall event to determine total volume of stormwater runoff for design events. The treatment design event used to size the wetpond was the 6-month, 24-hour storm event with a total precipitation of 1.28 inches.

Low Impact Development Assumptions:

- 1. Basin area values are based on the Low Impact Site Plan developed by AHBL.
- 2. All roof drainage and road runoff is routed through a network of swales and rain gardens with a total flow length of greater than 50-feet prior to discharge to detention ponds.
- 3. The rain gardens provided and grassed swales meet the minimum requirement for runoff treatment.
- 4. Due to flow length through vegetated areas, all roof area is modeled as grass.
- 5. Open space retained on the site is in forested conditions.

Method of Analysis

- 6. The site is divided into four basins (see Attachment #2). Each basin has its own stormwater quantity control facility.
 - a. Basin B1 is the northern portion of the site. This basin sheet flows towards the west. The western portion of this basin has been left undisturbed to allow for dissipation of stormwater runoff into the natural forest. This basin does not meet the DOE requirement for full dispersion. To obtain the full dispersion credit, eliminating the need for quantity control ponds, the basin must be 65-percent undeveloped and the total impervious area must be less than 10 percent of the basin area. Currently, as shown, Basin B1 is 55-percent undisturbed. This does not meet DOE requirements, therefore; a stormwater detention pond was developed for this basin.

- b. Basin B2 is the southwest portion of the site. This basin sheet flows across the southwest corner of the site and is partially intercepted by the ditch adjacent to 152 Street E.
- c. Basin B3 is the wetland and buffer area and the portion of the site directly tributary to the wetland through sheet flow. It was assumed that this basin in the developed conditions would be allowed to discharge directly to the wetland because we have reduced the area tributary to the wetland and the developed area tributary to the wetland consists of lots and undisturbed open space. All roof runoff will be sheet flowed or flow in swales for a minimum of 50-feet prior to discharge to the wetland buffer.
- d. Basin B4 is the southeast portion of the site. This basin sheet flows across the eastern property line.
- 7. The four Basins were analyzed for ten scenarios, each using a different combination of low impact development concepts. The model scenarios are described below: (the scenario numbers correspond to row numbers listed on Attachment 1)
 - a. Scenario #1 In Scenario #1 it was assumed that all roads would be 24-feet wide with asphalt concrete surfacing. Runoff is collected in a network of vegetated swales and conveyed to a stormwater quantity control facility. Rain gardens are provided for each lot or two lots share a common rain garden. By use of rain gardens and vegetated swales, it was assumed that the house roof area may be modeled as grass and not impervious surface. As stated earlier, undisturbed areas are assumed to be in a forested condition.
 - b. Scenario #2 Scenario #2 is set up the same as #1 except the roads are 20-feet wide.
 - c. Scenario #3 Scenario #3 is set up the same as #1 except the 24-foot roads are constructed of a pervious pavement system. The credit for pervious pavement is equal to the maximum credit allowed by the WWHM.
 - d. Scenario #4 Scenario #4 is the same as #1 with the addition of Pin Foundation systems. Based on the analysis by Rick Gagliano of Pin Foundations Inc., it was assumed that on average 47.7 percent of the undisturbed soil profile under a house would be 'activated' by the use of pin foundations. Pin foundation systems are constructed so that the majority of the natural soil profile is maintained under the house. Runoff from the house's roof is directed onto the lot and is allowed to flow through the soil profile under the house. The term 'activated' refers to the portion of the soil profile that is left undisturbed to which runoff from downspouts can be directed. The percent of activated soil under the house if a function of site topography, house configuration, and downspout location. It was assumed that the 'activated' soil profile could be modeled as pasture. Therefore, in the scenarios where pin foundations are utilized, it is assumed that 47.4-percent of the roof area may be modeled as pasture. In Scenario #4 the remaining

Row #	Raein	ă	&	· ·		
*		.0	7 5.	B3	2	Total Volume (ff*)
~	24-foot Road	32,600	27,743	•	20,577	80,920
8	20-foot Road	29,881	25,434	· · · · · · · · · · · · · · · · · · ·	18,864	74,179
က	24-foot Pervious Pavement	29,636	25,221		18,706	73,563
4	24-foot Road/Pin Foundation	29,606	25,195		18,687	73,488
w	24-foot Perv./Pin Foundation	26,621	22,655		16,803	66,079
9	24' Road/Pin 52.3% Impervious	39,991	34,033		25,242	99,266
~	24-foot Road/Imperv. Roofs	48,730	41,478		30,764	120,972
6 0	24-foot Perv, Pvmt. As Grass	20,766	17,672	-	13,107	51,548
Q	20' Perv/ Pin Foundation	24,446	20,804		15,430	60,681
9	20' Perv &s Grass/ Pin Found.	17,496	14,889		11,043	43,428
	Conventional Development	Detention Storage		Wetpond Storage		
		222,590		47,480		270,070

* assumes 47.7-percent of roof area can be modeled as pasture

⁻ values in shaded boxes have been computed based on percentages established by Basin B2 and not on actual model iterations.

⁻ area input values for the conventional development analysis are from the Pierce County Low Impact Development Study by CH2MHILL, dated April 11, 2001.

⁻ Wetpond assumed for treatment in conventional development. Design volume based on single event model. Revised 12/20/01

